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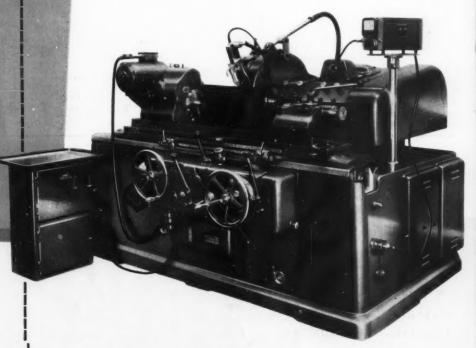
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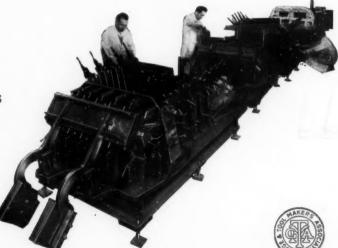
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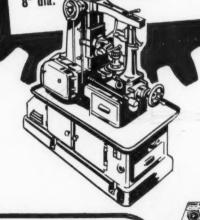
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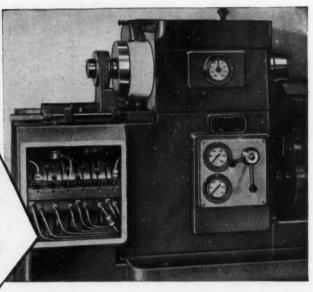
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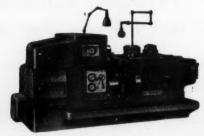
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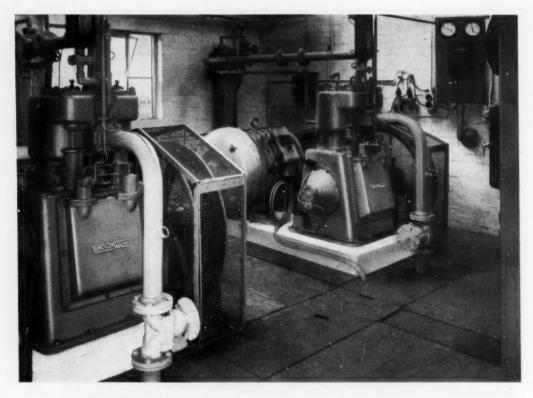
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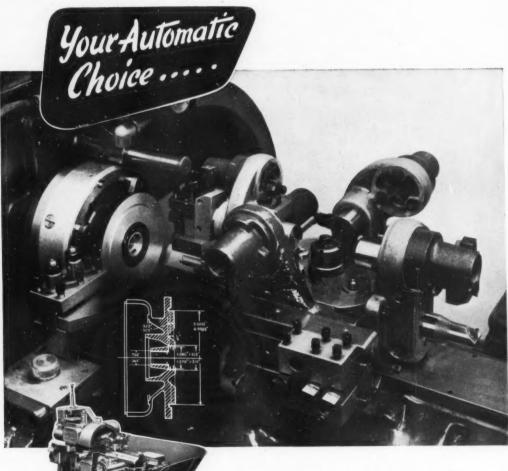
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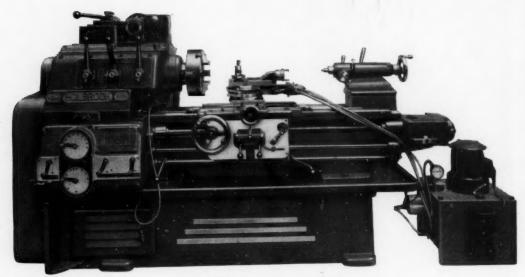
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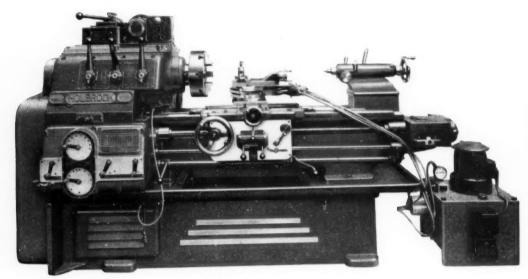
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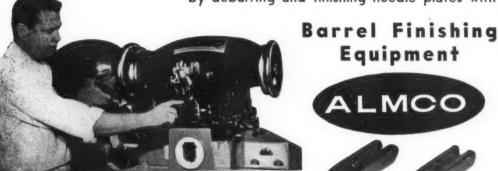
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DEVELOPMENT ENGINEER AT LANDIS MACHINE CO. REPORTS . . .

#### "We cut costs from £20 to 4/- per 100"

by deburring and finishing needle plates with



Mr. James W. Dunford, development engineer at Landis Machine Co. points to location of needle plate in new model of Landis shoe repair machine.

ALMCO

Equipment



REFORE

One of the most successful barrel finishing applications on record at Almco is this needle plate deburring and finishing at Landis Machine

The needle plate forgings are drilled and broached and then carefully deburred and finished. Formerly the cost of finishing and removing the tough burrs by hand filing was £20 per 100.

Now, an Almco Model DB-200 barrel finishing machine performs the same operation at a cost of 4/- per 100, a savings of 99%!

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By keeping simple records on processing cycles. correct media and compound, and proper scheduling, Landis engineers can switch the Almco equipment from part to part, to meet plant production requirements exactly.

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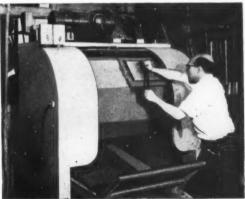
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#### MANY LANDIS PARTS NOW BARREL FINISHED

With this £1,143 annual saving on needle plates alone in mind, Landis engineers have applied the Almco method to other parts until the company is now barrel finishing several hundred different parts to high quality standards. Rejects are practically non-



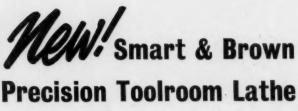
Finishing department operator at Landis Machine Co. gets ready for parts deburring run in Almco barrel finishing machine. Almco construction is heavy-duty throughout, to stand up under rugged requirements month after month.

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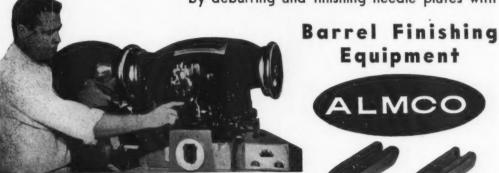
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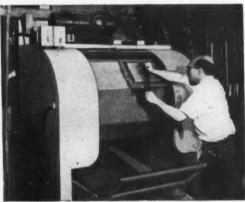
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Finishing department operator at Landis Machine Co. gets ready for parts deburring run in Almoo barrel finishing machine. Almoo construction is heavy-duty throughout, to stand up under rugged requirements month after month.



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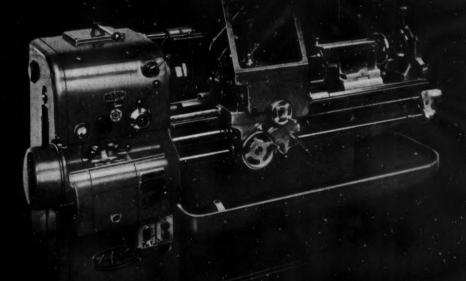
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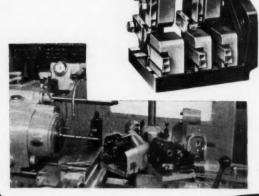
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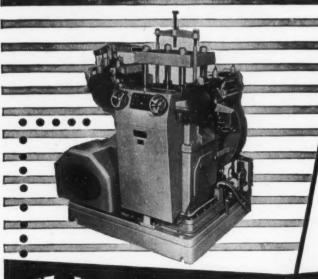
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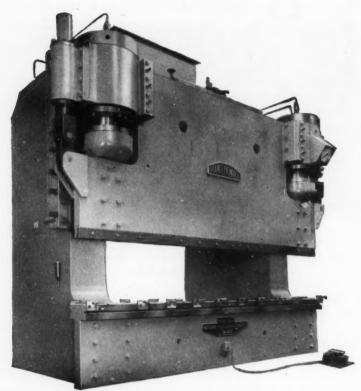




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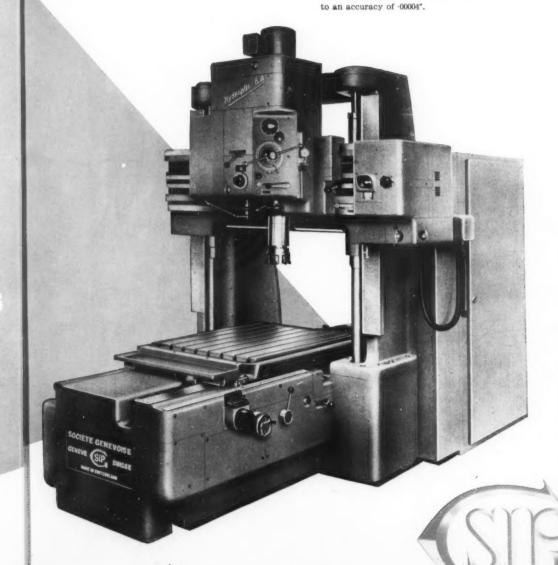
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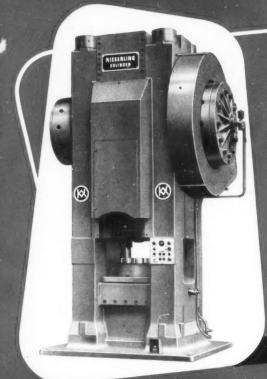
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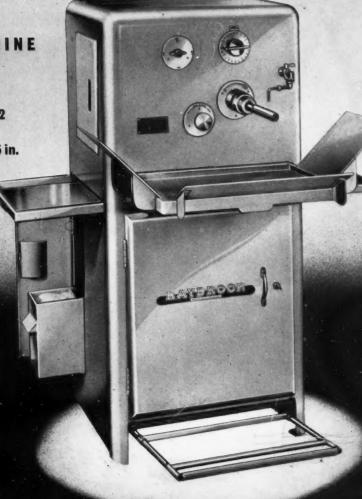
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HONING MACHINE

M O D E L 3 1 2 Capacity: ·120 in. to 2·625 in.





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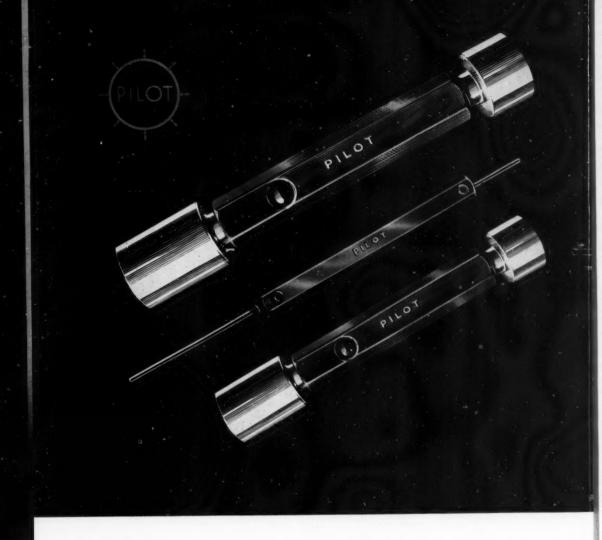
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Automatic clamping and unclamping of the slides

Electro-hydraulic control

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Light precision milling if required

Rotary table 16" x 16" optional

Brief specification	n :-		Mod	el B57
Dimensions of table			 	26° x 20°
Longitudinal stroke			 	20"
Transverse stroke			 	12"
Vertical stroke			 	12"
Feeds (stepless) ins/s	min.		 	2-112
Spindle speeds, r.p.n		steps)	 	48-4000

This hydraulically-operated machine, built by an oldestablished Swiss company to traditional Swiss standards of precision, is an economical production jig borer suitable for "one-off" or series production, without the need for costly jigs and fixtures.

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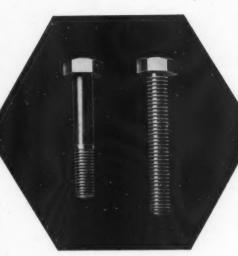


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OF CORRECTION REQUIRED
AT INDICATED ANGULAR
POSITION IN THE SELECTED PLANE



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Balancing is a process whereby the distribution of mass in a rotor is altered to eliminate vibrations at the supporting bearings. To statically and dynamically belance a rotor, a balancing machine must indicate the amount and the angular location for correction of mass or weight required in each of two planes perpendicular to the axis. Gisholl Type S Balancers provide these indications—quickly.

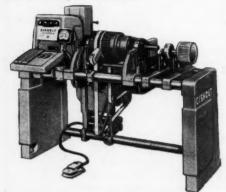
TWO OPERATING
CONTROLS: THESE
SWITCHES ARE FOR
INDICATIONS OF
UNBALANCE IN EACH Gishoit Dynetric Balancing machines and depicts Type 15B
PLANE OF CORRECTION
(BENCH model) for measuring and locating dynamic and
static unbalance (either or both) causing vibrations from

A STROBOSCOPIC
LAMP "STOPS"
A REFERENCE
NUMBER ON
THE BAND TO
INDICATE THE
ANGULAR
DIRECTION FOR

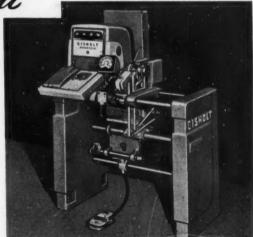
#### THE MODERN MEANS — Gisholt

The modern means for quickly and accurately measuring and locating unbalance in rotating parts is provided by GISHOLT balancing machines.

The Gishoft Machine Company (Great Britain) Limited, a subsidiary of Gisholt Machine Co., U.S.A., manufactures in this country the range of Dynetric type S horizontal dynamic balancing machines which handle work weighing from a fraction of a pound to 300 pounds and indicate, in each of two selected planes, the amount of correction material to be added or removed to obtain correct balance when vibrations at bearings are as small as 0.000025 in. and not more than 3/32 in. at bearings. When set-up the indication is given in only 15 seconds. Unbalance can be measured and corrected in the first of a new design of part in less than 15 minutes. The amount of correction may be read in any practical correction unit such as thousandths of an inch depth of drill or in 1/64 in. lengths of wire solder.



Type 315 for measuring and locating dynamic and static unbalance (either or both) causing vibrations from 0.000025 in., but not exceeding 3/32 in. at bearing surfaces of parts 24 in. max. dia., 24 in. max. length. Max. dia. at bearing surfaces: 2½ in. (weight capacity 2 to 50 lb.), or 5 in. (weight capacity 15 to 300 lb.), 1000 to 2000 r.p.m.



0.000025 in., but not exceeding 3/32 in. at bearing surfaces of parts from 1 to 30 lb., 12 in. max, dia, up to 12 in. max.

length, and 1\(\frac{1}{8}\) in. or less dia. at bearing surfaces. 1000 to 2500 r.b.m.

Type 1S (FLOOR type) same as 1SB, above, but including  $\frac{1}{2}$  H.P. enclosed motor with brake and control. This machine and its BENCH version can be arranged for parts  $2\frac{1}{6}$  in, or less dia. at bearing surfaces (weight capacity 2 to 50 lb.), alternatively  $\frac{1}{2}$  in, or less dia. at bearing surfaces (weight capacity 4 oz. to 5 lb.).

Standard machines can be arranged so that corrections for balance can be made in the balancer.

Gisholt, U.S.A., make a range of vertical Dynetric type S Balancers, a 'U' series for parts weighing from 25 to 300,000 lb., and special purpose balancing machines.

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For further details please write for publication 1/40

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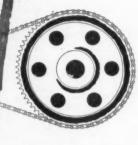
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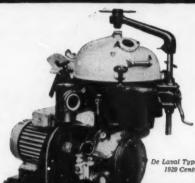
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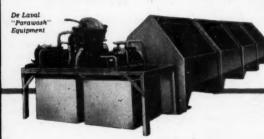
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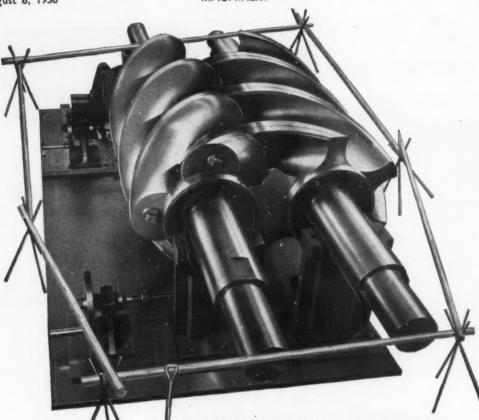


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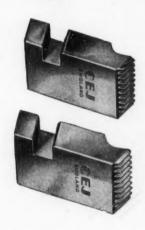
Plain and Screw Snap

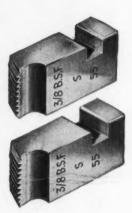
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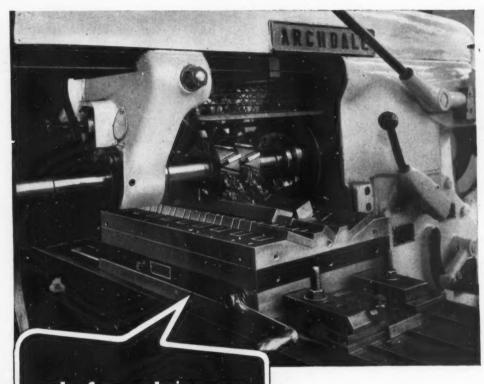
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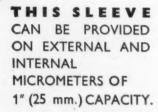
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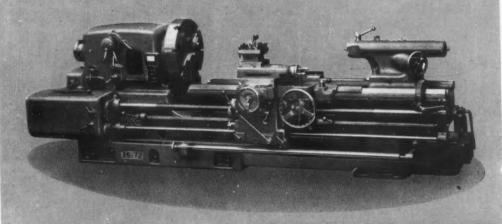
1958



..auxiliary feed change in apron

### ON 26" and 30" SWING LATHES

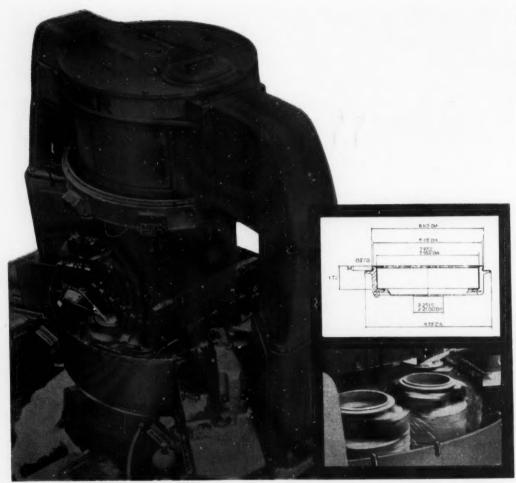
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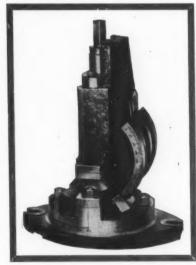
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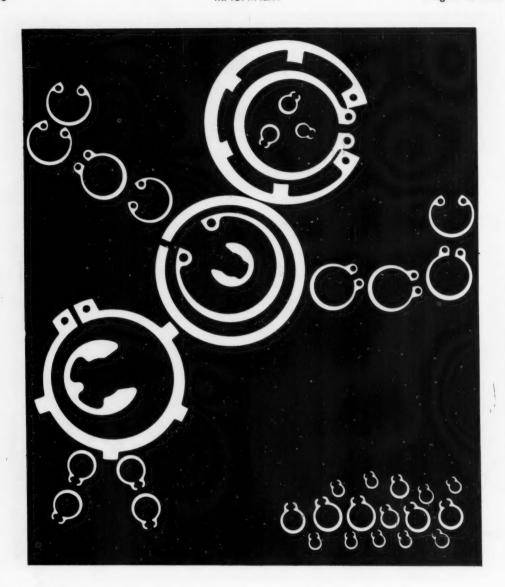
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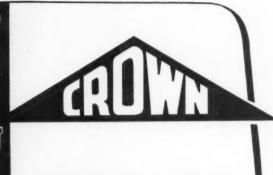
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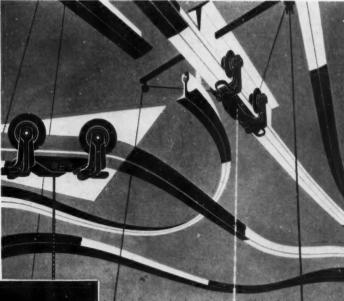
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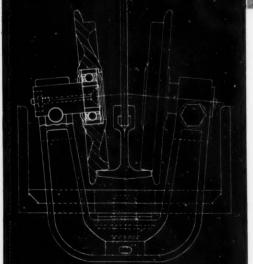
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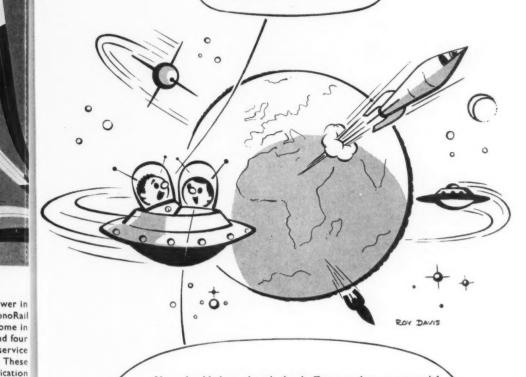
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- Cross feed 6½in., vertical 14½in., both hand.
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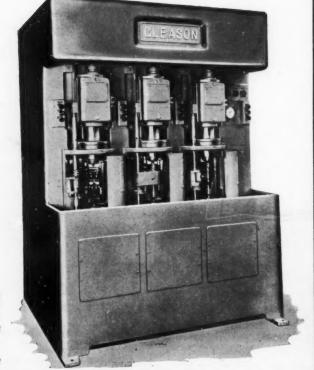
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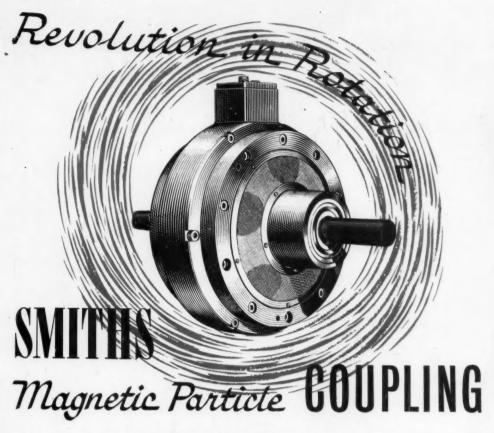
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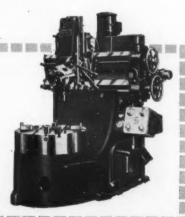
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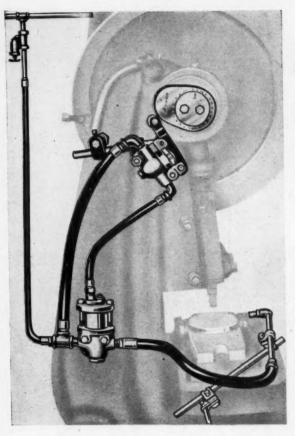
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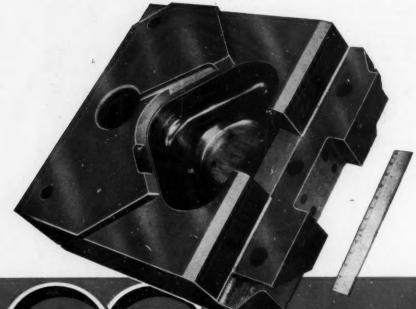
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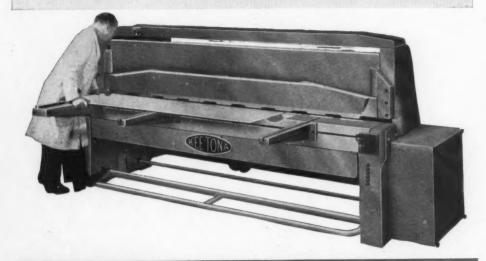
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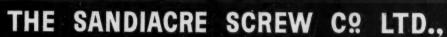
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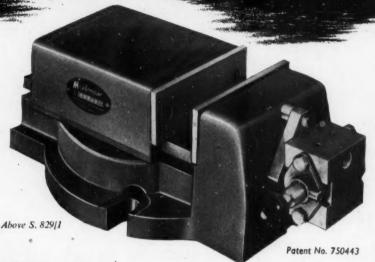
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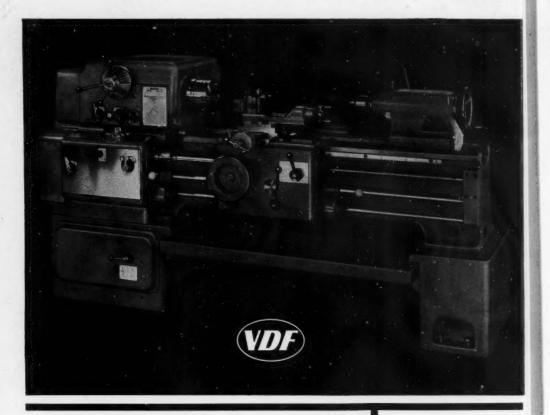


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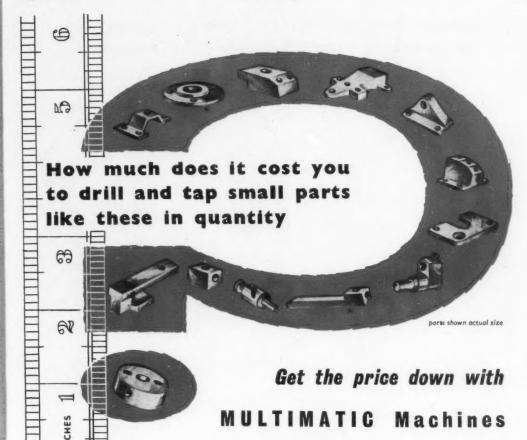
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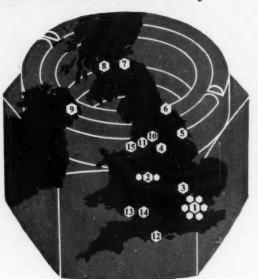
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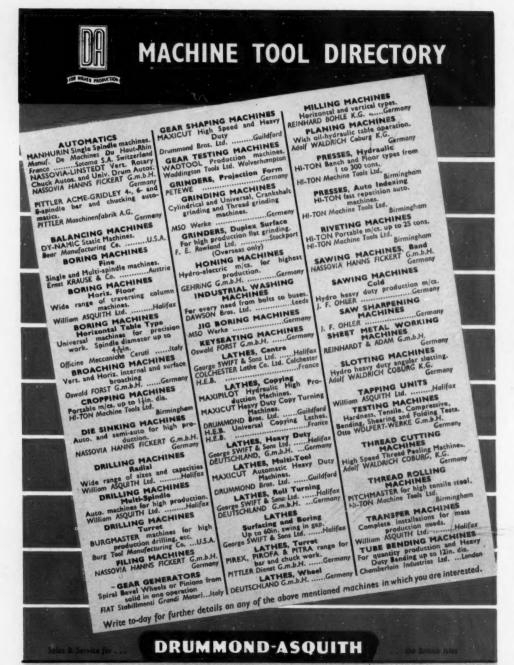
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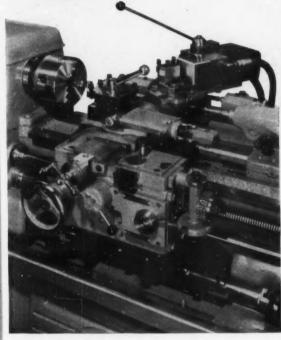


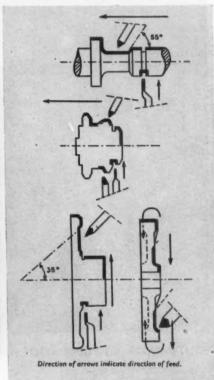
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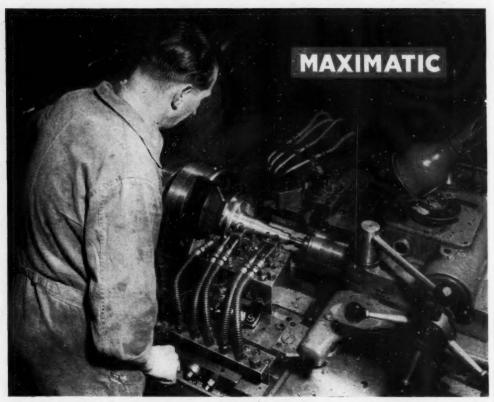
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# MACHINERY

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Vol. 93, No. 2386

Editorial

August 6, 1958

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(p. 285]F

# **Abstracts of Principal Articles**

### Aspects of Russian Engineering Industry P. 286

This article, the third in a series concerned with the engineering industry of the U.S.S.R., is devoted to the Sverdlov Machine-tool Plant, Leningrad, and the machine tools built therein. The plant builds a range of medium and heavy-duty horizontal boring machines, 3-dimensional profile milling machines and special purpose equipment, mainly for heavy industry. Recently, a programme control system has been developed in the plant, whereby co-ordinate settings can be made by "dialling" or from punched cards. This system has been applied to horizontal boring machines, and to a large jig-boring machine which is now in series production. The latter machine is of the portal type, with horizontal and vertical cutter heads, and it is stated that co-ordinate settings can be made to an accuracy of 2 microns (0.00008 in.). (MACHINERY, 93—6/8/58.)

# Automation Applied to Small-batch Production ...... P. 301

A line of three Kearney & Trecker machines installed in one of the plants of the Hughes Aircraft Co., U.S.A., is operated by the Digitape control system developed by the latter company. Intended for the production of parts in small batches, or even singly, the installation is so arranged that four different components may be in progress at any time, fixtures containing these parts being passed down the line in succession. One punched tape provides for all the operations on a given part and there are four tape readers. The first machine in the line enables milling operations to be performed in three directions at right angles. On the second machine there is an indexing turret which will accommodate a maximum of 20 different tools. These tools are brought to the operating position automatically and the quills are guided on an outboard support. There are two boring spindles on the third machine, one of which can be adjusted automatically for hole diameter. (MACHINERY, 93—6/8/58.)

### Peenamatic Shot Peening Machine for Forming Integrally-stiffened Wing Panels P. 311

Supplied by the Metal Improvement Co., U.S.A., to the Boeing Airplane Co., the machine described has a capacity for handling wing panels up to 84 ft. long by 7 ft. wide, and skin thicknesses up to  $\frac{8}{8}$  in. can be treated. The stationary work table is inclined at 30 deg., in the transverse plane, to facilitate recovery of the spent shot. Peening carriage traverse speed may be steplessly varied from 6 to 60 in. per min. Ten nozzles are adjustably mounted on a carrier which is reciprocated transversely while the operation is in progress. To enable the curvature of the work surface to be controlled, provision is made for adjusting the air pressure, and consequently the peening intensity, for each nozzle independently. (MACHINERY, 93—6/8/58.)

### 

With the aid of equipment here described, plungers for fuel injection systems are ground to a close fit for the cylinders on a Brown & Sharpe No. 5 plain machine. Setting for parallelism is made with the aid of an Electralign instrument for electronic alignment of the swivel table. For accurate size control an electronic caliper gauge is employed in conjunction with Ceda/Size equipment which provides a very fine feed of millionths of an inch per work revolution during the final stage. When mating parts are being ground, the equipment is used in conjunction with an Electromate attachment which incorporates a "computer-selector" unit. It is stated that clearance between piston and bore can be held within  $\pm 0.00002$  in. provided that the bore sizes do not vary by more than 0.0002 in. on diameter. (MACHINERY, 93–6/8/58.)

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# Kendall & Gent 300-ton Plano-milling Machine ...... P. 315

The machine here described has been installed in the Larne works of the British Thomson-Houston Co., Ltd. It has a capacity for work up to 29 ft. 9 in. by 12 ft. by 8 ft. 6 in. high. There are two vertical milling heads, each driven by a 60-h.p. variable speed motor, and provision has been made for fitting a horizontal milling head, if required. An Asquith drilling and boring head is mounted at the rear of the cross rail, so that various operations can be carried out on large workpieces with a minimum of handling. Feed rates for the table and milling heads range from  $\frac{1}{2}$  to 24 in. per min. (MACHINERY, 93—6/8/58.)

# Investigation of Chatter on Radial Drilling Machines ...... P. 317

It is pointed out in this article that chatter is normally induced as a result of vibration generated directly by machining. Attention is then drawn to two methods of vibration testing of drilling machines, one of which involves drilling under closely controlled conditions, and the other, the application of artificial loads by means of an electromagnetic vibration generator. The design and application of a suitable generator are briefly discussed, and vibration measurement and modes of vibration in radial drilling machines are then considered. Finally it is explained how this information may be applied to modify machine designs and to avoid operating conditions which are known to produce instability. In conclusion it is pointed out that the simulated tests with a vibration generator enable the effects of a wide range of frequencies to be rapidly investigated. (MACHINERY, 93—6/8/58.)

### IN FORTHCOMING ISSUES

Aspects of Russian engineering industry—The Triulzi factory for die casting and injection moulding machine production.

# **Developments in Tool Servicing Arrangements**

Cemented carbide cutting tool materials of various grades are now very widely employed and it seems probable that tools of ceramic-or sintered oxide as it should, perhaps, preferably be termed-will find rapidly increasing application in the future. The basic advantages of these materials are, of course, that they offer high heat and wear resistance, and when they are employed under suitable conditions, rapid metal removal rates can be obtained on the one hand, while, on the other, close dimensional limits can often be maintained over comparatively long runs. In this connection, however, it should be borne in mind that because very high cutting speeds are possible with the newer materials, and may even be essential for their satisfactory performance, a considerably increased length of run, expressed in terms of the number of components machined, may, in fact, be completed in less time than the former, shorter, run that was obtained with the tools previously employed. In other words, if the latest types of cutting tools are being used to the best advantage, when all factors are taken into account, it does not follow that their adoption will necessarily decrease-indeed it may possibly increase-the number of times that servicing is required per shift or per week.

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The newer tool materials, as is well known, are much more sensitive to operating conditions than is high-speed steel, for example. They are, perhaps, even more sensitive to servicing methods, and unless re-sharpening is carried out in such a manner that the material is not adversely affected, and the required geometry and surface finish are consistently obtained, optimum tool life and work quality cannot be expected. At the same time, it is becoming increasingly important that the time during which a machine is idle while one or more tools are being replaced should be kept to a minimum. Obviously, the shorter the machining cycle, the greater is the loss of output when the operation

is interrupted for a given period.

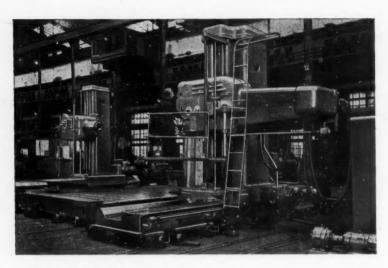
One method of simultaneously ensuring consistent servicing and reducing idle time is to employ clamped, "throw-away," tips of carbide or ceramic. The advantages of such tips have frequently been discussed, and it appears that they have found wide and constantly increasing application, particularly in the U.S.A., not only for single-point turning tools, but also for milling and boring

operations. In the circumstances the apparent lack of enthusiasm of many British manufacturers towards this development is difficult to understand. Such tools, it might be thought, should be of special interest to smaller firms which have not hitherto employed carbide—or sintered oxide—because they have been reluctant, or unable, to provide the necessary grinding and lapping equipment for servicing on the very limited scale that would be involved.

Where throw-away tips are unsuitable or are not yet being employed, the user of carbide or sintered oxide is now afforded a considerable choice of equipment whereby correct sharpening of tools is greatly facilitated. For example, in addition to conventional grinding and lapping machines of the face-wheel type, with provision for accurate control of angle, there are machines which provide for simultaneous rotary and oscillating motions, or reciprocating motions only, in one or two directions. Mention may also be made of abrasive band type equipment, and spark erosion machines which are claimed to avoid the formation of incipient cracks in the tool material.

Proper tool sharpening is an essential part of an effective servicing system, but there are two other aspects which are of almost equal significance. If the best results are to be obtained as regards both work quality and tool life-where tools are to be re-sharpened-it is essential that the tools should be removed from machines for servicing at regular intervals to avoid the destructive effects of continued operation after the edges have become dulled. Depending on the complexity of set-ups or installations, various arrangements may be adopted to ensure systematic tool replacement. For use with elaborate transfer machines, the value of dials which indicate when individual tools have completed their allotted numbers of operations has been fully established. It is a simple matter, moreover, to arrange for the machine to be automatically stopped for tool changing so that the dials need not be kept under frequent observation. As a contribution to the attainment of maximum quantity and quality of output, it may well prove desirable in the future to employ such tool control boards on an increasing scale for other types of machines, notably multi-spindle automatics and multi-tool lathes.

(Continued on page 334)



# **Aspects of Russian Engineering Industry**

Some Impressions Based on a First-hand Study of Soviet Plants

Earlier articles in this series\* on some aspects of the engineering industry in the U.S.S.R. were concerned with the growth of the Russian machine tool building facilities, and some recent Soviet machines were described and illustrated. The Ordzonikidze Machine Tool Plant, in the suburbs of Moscow, was considered in some detail, and it may be recalled that this plant is engaged in the building of multi-spindle automatics and hydraulic copying lathes, also in the design and construction of special-purpose and automatic transfer machines. Another Soviet machine tool plant will now be described, namely, the Sverdlov works, in Leningrad, where boring machines and special-purpose equipment are built.

### SVERDLOV MACHINE TOOL WORKS

The Sverdlov Machine Tool Works is stated to be the longest-established plant for building machine tools in the Soviet Union. Before the revolution, there was an engineering factory on the present site, owned by a German company. This factory was engaged principally in the production of diesel engines, but some machine tools were built. It was closed down in 1917, and did not re-open until 1925, when it was planned to specialize in the building of metal-working equipment. Initially,

the output consisted solely of lathes, but since that time, many different types of machines have been built, including shapers, boring machines, polishing machines and special-purpose units. In 1932, the decision was made to concentrate mainly on the construction of boring and copy-milling machines, although the building of other types of metal-cutting equipment was also undertaken. During the second world war, the plant continued to build machine tools, until it was demolished by eight direct hits during bombing raids. Every effort was made to rebuild the works as quickly as possible, reconstruction proceeding shop by shop, and, before the end of the war, production was resumed.

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Some 2,500 people are now employed at the Sverdlov plant, and the technical, engineering and design staff total 500. More than 30 per cent of the latter are women, the greater proportion of whom are designers or technologists. Many of the designers and engineers have been working at the plant for 15 to 30 years, and the chief engineer started at the plant as a turner, 30 years ago, pursuing his technological studies in his spare time. A close connection has always been maintained between the Sverdlov plant and the Leningrad Special Technicum for Machine Tools, and it may be of interest to note that the principal of this technicum, Professor Sukolov, started his career as a bench hand at the plant.

<sup>•</sup> MACHINERY, 93/4-2/7/58, and 93/137-16/7/58.

The Sverdlov works has a very strong technical team, which includes four Candidates of Technical Science—a qualification that ranks immediately below a Doctor's degree—and the overall experience of this team is very wide. Liaison is maintained with the various Soviet machine-tool research institutes, such as ENIMS, and these institutes collaborate with the plant to solve any particularly difficult design problems. It is stated that the design and technical staff of the plant seldom have to call on outside help, and, in many instances, assist the institutes in their work.

All the design and development work associated with machine-tool building is carried out by the plant's own staff. There are four design offices, all equipped with draughting machines, each office specializing in a particular field of design, namely, boring machines, milling machines, automatic and special machines, and electrical systems. These offices are served by a separate calculations bureau. From 30 to 35 different types or sizes of machines are built each year, including special machines for the production of turbines and equipment for the heavy industries. Since 1945, the output of the plant has been increased by approximately 24 times, as indicated by the chart, Fig. 1. This expansion has been brought about by the introduction of new and more efficient equipment and methods, and improvement in labour efficiency, as can also be seen from the chart. In the future, it is planned to increase output by 12 to 15 per cent each year. At present, about 15 per cent of the production of the plant is being exported to such countries as Finland, Switzerland, Îndia and Japan, in addition to China and other countries in the Soviet bloc.

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A large number of the machines in the plant are of American or British origin, but these units are gradually being replaced by Russian-built equipment. Some of the older foreign machines have been modernized. Generally, the amortization period for equipment is eight to ten years, but last year some 60 lathes were replaced which were only about five years old, since greatly improved types had become available. Finance for the provision of new equipment is obtained from two sources. One, is by borrowing from the State bank, which advances loans over a period of two years without interest. The other source is the "director's fund." In common with other Soviet plants, the Sverdlov works pays a fixed proportion of its annual profit to the state. The remainder forms the director's fund, and is used by the plant for the purchase of new equipment, improvement of the housing facilities provided by the plant, and for the betterment of the working conditions and amenities. In a well-run plant, it is stated, about 40 per cent of the director's fund is used each year

for the purchase of new production equipment. During 1957, the Sverdlov works was able to transfer 1,600,000 roubles to the director's fund, of which 300,000 roubles was devoted to housing and improving working conditions, and the remainder was spent on new equipment.

The plant occupies an area of about 740 acres. There is an extensive main production shop, which is divided into three bays, one for machining spindles and smaller details, another for operations on heavy castings, and the third for machining castings of medium size. The plant has its own foundry for small castings, but, at the time of our visit, all other castings were obtained from outside sources. A large conveyorized foundry is to be laid down next year. A unified system of machine construction is applied wherever possible, with components that are common to a number of machines, and it is claimed that, generally, about 80 per cent of the parts used on any one machine are also used on other machines built by the plant.

### BORING MACHINE DESIGNS

As has already been intimated, by far the greater proportion of the output of the Sverdlov plant consists of horizontal boring machines. The type 262G was introduced in 1946, and has been in full production for the past ten years. It is of conventional design, and, like all Russian horizontal boring machines, has the headstock at the right-hand end

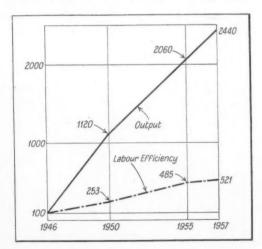


Fig. 1. Increases in Output and Labour Efficiency at the Sverdlov Machine Tool Works, Leningrad, during the Post-war Years, are Indicated by these Graphs

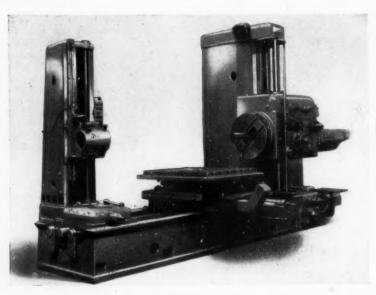


Fig. 2. The Sverdlov Type 2620A Mediumduty Horizontal Boring Machine, which will be the only Medium-duty Design Built by the Plant after the end of this Year

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of the bed, as viewed from the front. The machine table measures 1,000 by 800 mm. (40 by 35 in. approximately), and the main spindle is of 85 mm. (3.346 in.) diameter. Spindle speeds range up to 1,000 r.p.m., and the facing slide has a maximum travel of 150 mm. (5.9 in.). Two other horizontal boring machines have been developed from this basic type, one of which—the type 262D—has a spindle of 110 mm. (4.331 in.) diameter, without a facing slide, but is similar in all other respects to the earlier machine. The 2621 boring machine, is similar to the 262G type, but has a maximum spindle speed of 2,000 r.p.m., and no facing slide, and production of this machine started in 1950. About 70 per cent of the plant's current output of 350 medium-duty boring machines per year consists of these three types, the remainder comprising the latest design, type 2620A.

Shown in Fig. 2, the type 2620A was introduced early this year, and next year the plant will only build this one type of medium-duty machine. It has a main spindle of 90 mm. (3·543 in.) diameter, which is bored No. 5 Morse taper, and the maximum axial travel of the spindle is 710 mm. (27·953 in.). The face-plate is 625 mm. (24·606 in.) diameter, and has a facing slide with a maximum travel of 170 mm. (6·693 in.). To ensure long working life, the boring spindle is nitrided, and runs in precision roller bearings. There are 22 spindle speeds, ranging from 12·5 to 2,000 r.p.m., and 15 speeds for the face-plate, from 8 to 200 r.p.m. A 2-speed motor, of 10/13·5 h.p., is

used for the spindle and face-plate drive, the motor speeds being 1,500 and 3,000 r.p.m., and all speeds are selected by single-lever control. Special provisions have been made in the headstock gearbox to prevent excessive wear and damage to the ends of the gear teeth.

Workpieces weighing up to 2 tons can be sup-

ported on the rotating table, which has a working surface measuring 1,120 by 900 mm. (44 by 35½ in.). The table has maximum traverses of 1,150 mm. (4514 in.) in the longitudinal direction, and 1,000 mm. (39% in.) crosswise. The boring spindle and the outboard support bearing can be elevated from 0 to 1,000 mm. above the working surface of the table. Steplessly-variable rates of feed are provided for the table (longitudinally and transversely), the headstock and support bearing (vertically), the spindle (axially) and the facing slide (radially), by means of an amplidyne system. Indicators are fitted which show the feed rates in mm. per rev., and these rates range from 1.4 to 1,110 mm. (0.055 to 43.701 in.) per min. for the table and spindle head, from 2.2 to 1.760 mm. (0.087 to 69.291 in.) per min. for the spindle, and from 0.88 to 700 mm. (0.035 to 27.559 in.) per min. for the facing slide. All these members can be rapid-traversed, the rates being approximately double the normal maximum feed rates. The maximum feeding force that can be applied is 1,500 kg. (3,300 lb.), the maximum torque at the spindle is 223 lb./ft., and the maximum torque at the facing slide is 323 lb./ft. Threads can be cut with Metric pitches ranging from 1 to 10 mm., the range of English threads being from 4 to 20 per in.

An optical measuring system is provided for co-ordinate setting, measurements being made with the aid of projection screens, from master scales with 0·01-mm. (0·0004-in.) divisions. All moving elements are clamped in two mutually-perpen-

dicular planes, in order to reduce the effects of working clearances and their attendant errors. All motions are controlled, and speeds and feeds are selected, from the main panel on the headstock, through an electrical system, and there is an auxiliary panel, for remote control, mounted on the column for the outboard support bearing. The machine weighs approximately 13½ tons, and is 18 ft. long, 10 ft. wide, and 10 ft. high.

A larger horizontal boring machine, of a similar design to the type 2620A has been developed, and individual machines are now being built. This borer has a table measuring 1,600 by 1,250 mm. (63 by 49 in.), and is provided with a large-screen optical measuring system. The spindle is of 125 mm. (4921 in.) diameter, and the maximum spindle speed is 1,200 r.p.m. It may be of interest to note that series production of this machine is to be undertaken by the Komsomolensky Machinetool Plant.

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### HEAVY-DUTY HORIZONTAL BORING MACHINES

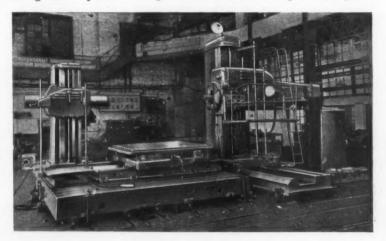
The larger boring machines in the Sverdlov range are built to order, and one of these heavy-duty machines is shown in Fig. 3, at the end of one of the shops of the Leningrad plant. This machine is designated type 2657C, and incorporates four main units, which are separately mounted, namely, a baseplate, a traversing column and head assembly, a table assembly, and an outboard support. When required, the table assembly can be removed, and workpieces are then mounted directly on the baseplate. The main column can be traversed on vee and flat guideways, and the headstock has a main spindle of 150 mm. (5-905 in.) diameter, also a facing slide. Spindle

speeds are electronically controlled, and are steplessly-variable up to 1,000 r.p.m., the speed in use being indicated by means of a dial on the head-

Measuring 2,250 by 1,800 mm. (88½ by 70% in. approximately), the table has longitudinal and rotary motions only. Rate of traverse of the table, also of the headstock vertically, the spindle longitudinally, the facing slide radially, and the column transversely, are steplessly-variable, and are regulated by means of a special electronic control system that has been developed in the Sverdlov plant. Control is effected by movement of a single, handactuated star-wheel, and the traverse rates can be varied steplessly in a ratio-range from 1:1 to 1:1.800. The actual feed rates depend on the requirements of the particular unit that is to be moved, and on the gearing employed. Under amplidyne control, the constant-torque, variablespeed motor provides input speeds ranging from 2 to 3,600 r.p.m., and, with suitable gearing, one group of feed rates may vary from 0·1 to 180 mm. per rev., for example. This Sverdlov system, it may be noted, is widely used on machine tools built by other plants in the Soviet Union.

There is a heavy-duty boring machine of generally similar design to the type 2657C, but with a column and bearing support that are fixed in position transversely but are movable longitudinally, and a table that can be traversed cross-wise. The type 2656C machine, seen in the heading illustration, has a fixed baseplate and traversing column. Of 175 mm. (6.889 in.) diameter, the spindle of this machine can be run at a maximum speed of 1,000 r.p.m., and the same method of feed control is employed. A large traversing-table boring machine is shown in Fig. 4. Designated

Fig. 3. This Large Horizontal Boring Machine, Seen at the End of One of the Shops in the Leningrad Plant, Comprises Four Separate Units, which Can be Used in Combination or Separately, as Required



type LR66C, this machine has a table measuring 5,000 by 2,500 mm. (16 by 8 ft. approximately), and a 150-mm. (5·905-in.) diameter spindle that can be run at a maximum speed of 1,000 r.p.m. The crosswise travel of the table is 5,000 mm., and it is supported on the vee and flat guideways of the bed for the whole of this movement. The Sverdlov feed control system is again employed, and the travel of the various members is indicated by large dials, one of which can be seen at the right-hand side of the headstock, and another on the column base. This machine weighs 55 tons, complete.

### COPY-MILLING MACHINES

A number of different copy-milling machines is made at the Sverdlov plant, and the type 6441B semi-automatic machine is shown in Fig. 5. In principle, this unit is similar to the Keller machines, the master and work being mounted one above the other, and the master being scanned by the stylus of an electrical follower unit on top of the cutter head. The electrical control system provides for full 360deg. copying, the motions of the cutter spindle, spindle head, and work table being engaged by electro-magnetic clutches. Workpieces measuring 900 by 500 mm. (35½ by 19% in.) can be machined, and the maximum depth that can be milled is 300 mm. (1113 in.). Spindle speeds up to 3,100 r.p.m. can be employed, and the maximum traverse rate for copying is 315 mm. (12.402 in.) per min.

A larger machine, of generally similar design, is built, and is designated type LR105. Workpieces measuring 1,400 by 800 mm. (55% by 31½ in.) car

be machined, to a maximum depth of 800 mm., and the spindle speeds range up to 3,150 r.p.m. The largest Sverdlov copy-milling machine—type LR29—will mill workpieces measuring 3,200 by 1,800 mm. (126 by 71 in.), and the maximum depth that can be machined is 1,000 mm. (39% in.). A new design was introduced last year, and differs from the other machines in that the maximum traverse speed for copying is 750 mm. (29.53 in.) per min. The spindle of this type LR93 machine can be run at 1,800 r.p.m., and workpieces measuring 2,250 by 1,120 mm. (88% by 44 in.) can be milled, to a maximum depth of 900 mm. (35% in.).

### SPECIAL MACHINE TOOLS

The building of special-purpose machine tools is an important activity of the Sverdlov plant. Single- and multiple-spindle boring machines have been supplied to works in the Soviet Union engaged in the production of motor cars, electrical equipment, and steam and electric locomotives, also to shipbuilding yards. Many of the special boring machines incorporate standard heads and other units developed by the plant, and a 2-spindle boring machine for operations on the housings of driving motors for electric locomotives is shown in Fig. 6. The complete machine weighs approximately 45 tons, and has two headstock units of standard design-one designated LR79A and the other LR79B. Both heads operate simultaneously, on an automatically controlled cycle, which is started by pressing a push-button on the control panel at the front of the machine. For convenience during setting, the complete panel can be removed

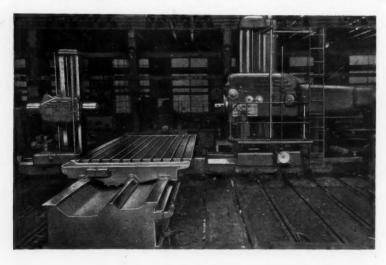


Fig. 4. Of the Traversing-table Type, the Sverdlov LR6oC Boring Machine, Here Shown, has a Spindle of Approximately 6 in. Diameter, which can be run at 1,000 r.p.m., and Incorporates an Amplidyne-drive for the Feed Motions



Fig. 5. A Range of Copy-milling Machines is Made by the Sverdlov Plant, and the Type 6441B is Here Shown. It Operates on a Semi-automatic Cycle, and has an Electrical Copying System

from its support, and moved to any position on the machine, to which it is connected by means of a long multi-core flexible armoured cable.

Two parallel bores are machined in the work-

pieces, which are mounted on their sides. Each workpiece remains stationary and is clamped in position by arms connected to an electro-mechanical system, which is controlled from the push-button panel. On either side of the work-support fixture there are pairs of massively-proportioned guide bushes, to support the boring bars. The two heads move on the vee and flat slideways of bed units at the right-hand end of the machine (as viewed in Fig. 6), and each is traversed by means of a short, driven screw, mounted below the head, which engages the teeth of a long half-nut, which is made in sections, and installed between the bed ways. Steplessly-variable feed rates are provided by an amplidyne system-similar to that already mentioned—and to facilitate setting, the position of the head is indicated by a large indicator dial at the lower right-hand end of the unit. The boring bars are arranged for radial adjustment of the cutting tools, and the mechanism is power-operated and push-button controlled. A second dial is mounted on the front of each headstock to indicate the radial position of the tool.

A larger machine, with two head units of greater capacity but generally similar design, has been built for line-boring operations on the main castings of diesel engines for locomotives, which may range up to 5 metres (16.4 ft.) long. Another special machine which has been built for diesel engine production is equipped with a tracer control system, whereby the workpiece is aligned automatically with the machine spindle in the various positions required for boring a number of holes. Special copy-milling machines have also been built, and one large unit, for the production of tyre moulds, will accept workpieces up to 9 ft. diameter.

Fig. 6. The Double-head Machine here shown is Employed for Boring Operations on Electric Traction Motor Bodies and has been Built by the Sverdlov Plant. It Incorporates Headstock **Units of Standard Design** which are Traversed by Short Screws and Long Half-nuts, Installed Between the Bed Ways

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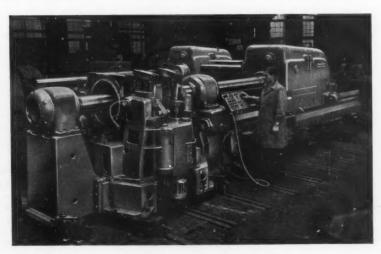
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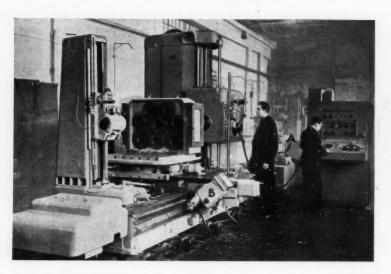


Fig. 7. The Numerical Control System Fitted to this Type 262PR Sverdlov Horizontal Boring Machine Provides for Co-ordinate Setting by "Dialling" or by means of Punched Cards. A Similar Machine is being Displayed in the Soviet Pavilion at the Brussels Exhibition

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### PROGRAMME-CONTROLLED BORING MACHINES

For a number of years, an increasing interest has been shown in numerically-controlled boring machines at the Sverdlov plant, and a number of different types have been developed. Fig. 7 shows a type 262PR horizontal borer which is arranged for numerical control, either by "dialling" or by the use of punched cards, and a similar machine is being shown in the Soviet pavilion at the Brussels exhibition. The machine is here seen in the course of trials at the Leningrad works. As may be observed, the design follows normal Sverdlov practice, and it has been developed from the type 2622, which has an optical measuring system. The programme control console is seen at the right, and it is connected to the machine by a multi-channel cable, so that it may be located in any convenient position. A separate card-reader, which is just visible at A, is employed when machining operations are performed under punched-card control.

The control system permits the pre-selection of the longitudinal and transverse positions of the table, and the vertical setting of the headstock, over the full ranges of travel, the units being moved automatically to the selected positions within an accuracy of  $\pm 0.05$  mm. (0.002 in.). Cutting speeds, feeds, and positioning rates can be pre-selected and changed during the machining cycle, at predetermined positions in the table and head movements. Information, in decimal form, is "dialled" by means of telephone-type units on the control console.

When punched-card control is employed, infor-

mation for ten positions of the table longitudinally and tranversely, and of the headstock vertically, can be recorded by piercing the card in accordance with a binary code. All the positional information, in decimal form, is "dialled" on the main console, and is automatically converted into a binary code and punched into the card. In the card-reader, the card is mounted on a stationary drum, which is swept by a series of contact members, carried by a rotating beam. These members sense the positions of the perforations as the beam travels round the drum. When required, the machine can be arranged to operate on an intermittent cycle, with pauses for tool changing, and it can also be employed for milling transverse faces on a workpiece, under automatic cycle control.

For co-ordinate setting, the machine is fitted with metal precision scales, graduated in increments of 1 mm. (0.0394 in.), and photo-electric sensing units. One such unit may be seen at B in Fig. 7, and provides for recording the longitudinal position on the table. Similar units are fitted for the transverse setting of the table, and the vertical setting of the headstock, but, for convenience, only the control of the longitudinal movement of the table will be considered. An image of the master scale is projected by means of an optical system on to a screen in the unit B, and a photo-electric cell in this unit senses the images of the scale-graduations, and transmits a signal to the control console, for each 1-mm. of table travel. When the table 'approaches the required setting, its rate of motion is gradually reduced, and it moves at a slow speed until it has completed the

nearest whole-millimetre distance that is less than the required dimension. Then, a fine-position unit is brought into operation, and this unit can be adjusted, by means of a servo-motor, relative to the main sensing unit, over a distance that corresponds to the pitch of the graduations on the scale-image projected on the screen. The fine-positioning unit incorporates a photo-electric cell and a special shutter mechanism which is opened at the completion of each 0.01-mm. (0.0004-in.) of table movement, to permit the passage of light from the screen to the photo-electric cell. The light pulses are converted into electrical signals by the cell, and these signals are transmitted to the control console, where they are counted electronically. The table continues to move at slow speed until the required number of signals have been received, corresponding to the decimal portion of the specified dimension, and is then stopped.

The 262PR machine has a spindle of 110 mm. (4·330 in.) diameter, which is bored for No. 6 Morse taper shanks, and has a maximum axial movement of 710 mm. (27·952 in.). Measuring 1,120 by 920 mm. (44 by 36 in. approximately), the table has a maximum travel of 1,150 mm. (45·275 in.) longitudinally, and 1,000 mm. (39·370 in.) transversely, and the spindle can be positioned vertically from 0 to 1,000 mm. above the table sur-

There are 22 spindle speeds, from 12.5 to 1,600 r.p.m., and the maximum torque that can be applied is approximately 2,900 lb.-in. feeds for the table and headstock range from 1.4 to 1,110 mm. (0.055 to 43.7 in.) per min., and for the headstock spindle from 2.2 to 1,760 mm. (0.087 to 69.3 in.) per min., the feed indicators being calibrated to read in mm. per rev. Threads from 1 to 10 mm. pitch, and from 4 to 20 t.p.i. can be cut, and the greatest weight of workpiece that can be mounted on the table is approximately 2 tons. The machine is driven by a 1,500/3,000 r.p.m. A.C. motor, of 10/13.5 h.p.

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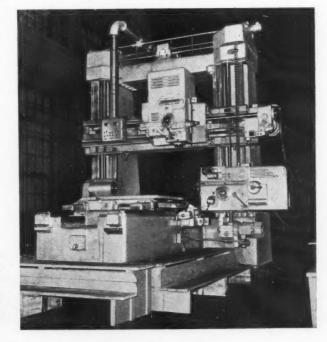
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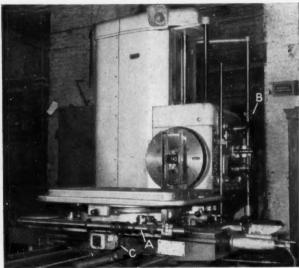
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Fig. 8. Large Jig-boring Machines of this Type are now in Series Production at the Sverdlov Works. It is Claimed that Co-ordinate Settings can be Made to an Accuracy of 2 microns (0.00008 in.), and a Machine of this Design is being Exhibited at Brussels

### LARGE JIG-BORING MACHINE

Large jig-boring machines (type LP87) are now in series production at the Sverdlov plant, and one of these machines is being exhibited at Brussels. Another is seen in Fig. 8, installed in one of the shops of the Leningrad works. Of the portal type, the machine has two spindle heads, one on the cross-rail, and the other on the right-hand upright, a support bearing for use with the latter head being carried on the left-hand upright. The heads are independently driven, and the maximum spindle speed is 1,800 r.p.m. An automatic levelcorrecting system is incorporated for the cross-rail, to ensure that the latter member is always parallel with the surface of the work-table. The table, which will support workpieces weighing up to 37 cwt., measures 2,200 by 1,400 mm. (6 by 4½ ft.). A separate electrical system is incorporated for the traverse motions which provides an excep-tionally wide range of feed rates, and permits "inching," under push-button control, in increments of 0.001 mm. (0.00004 in.). The optical positioning system for the table and spindle heads is stated to permit settings to be made within an accuracy of 0.002 mm. (0.00008 in.). With this system, enlarged images of the positioning scales are projected on to viewing screens for the heads





and table. All motions, and the selection of speeds and feeds, are controlled from a pendant panel, by means of push-buttons and selector knobs, as well as from the heads. The panel is carried on the lower end of a telescopic support-arm, of cranked shape, which is mounted on guideways above the main bridge structure. An individual motor is provided for traversing the arm, and is controlled from push-buttons on the panel. The machine, which weighs approximately 36 tons, can be provided with a programme-control system, similar to that already described, whereby boring operations can be performed from punched cards, or by "dialling."

### **WORKSHOP FACILITIES**

The various standard machines in the Sverdlov range are being built in batches, and, as might be expected, the production methods and equipment employed are conventional. Reliance is placed on accurate machining and fitting, and large numbers of general-purpose machine tools are installed in the Leningrad works. For the initial operations on the major castings, there are planing and plano-milling machines of various sizes, and many of these machines are American built. A Cincinnati Hypro planer was being used for finishing the slideway surfaces of bed castings, at the time that this article was prepared, and for this purpose a flat tool, about 6 in. wide was employed, with paraffin as a lubricant. A smooth, high-quality finish was produced, and the only subsequent

Fig. 9. The Prototype 2620A Horizontal Boring Machine, Here Shown, has been Fitted with an Electromechanical Positional Control System for the Table and Headstock

operation that was carried out was the mottling of the slideway surfaces with a scraper to ensure effective lubrication. This procedure is adopted for bed-castings up to 10 metres (32.8

ft.) long.

Among other American equipment was noted a large Reed-Prentice vertical milling machine, and King and Bullard vertical boring and turning mills. Although all the foreign equipment was fairly old, it appeared to be in good condition. All machines in the plant are systematically serviced, under a planned preventive maintenance scheme.

Extensive use is made of boring machines built in the plant, and many prototype machines have been installed in the Leningrad works in order that first-hand experience may be gained with regard to their performance under normal operating conditions, also to enable modifications and improvements to be carried out, which may be incorporated in later designs. In Fig. 9 is shown the prototype for the latest 2620A design, to which reference has already been made. This machine is generally similar to the production type, Fig. 2, but has been fitted with an electro-mechanical position control system for the table and headstock. Indexing stop-bars are provided for the table-saddle transversely, and for the headstock vertically, as indicated at A and B respectively. Eight stop units are slidably mounted on each bar, and each unit consists of two members, similar to bearing caps, which are provided with screws for clamping the assembly in any position along the bar. A lug on one member carries a screw, parallel with the bar, which provides a means of fine setting. The stops can be set at different angles on the bar, so that each screw, in turn, can be brought into alignment with a trigger that projects from a casing secured to the table-saddle or table. Each casing houses a limit switch, and the unit for the table-saddle is indicated at C, in Fig. 9. The limit switch controls an electro-magnetic clutch in the associated traverse drive mechanism, and when a stop engages the trigger, the limit switch is tripped and motion is stopped.

The first type 262G Sverdlov horizontal boring

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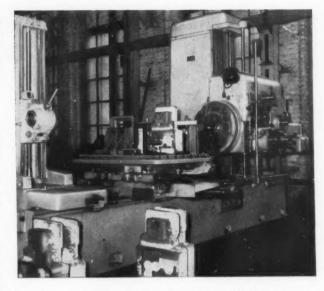
Fig. 10. This Prototype of the Obsolescent Type 262G Boring Machine has been Employed at the Leningrad Works for more than Twelve Years. Experience Gained from the Use of this Machine has Led to New and Improved Designs

machine to be built has been in use in the plant for more than twelve years, and is seen in Fig. 10 set up for boring cover castings for feed gearboxes. As these parts are for a machine that is not built in large batches, the castings are mounted on the boring machine table, with the aid of simple clamps and an angle plate, and each hole is bored individually. On the machine headstock, there is a large star-wheel for traversing the cutter spindle by hand, and in the centre of this wheel there is a single lever control for selecting

the speeds and feed rates, which are indicated on annular scales. In addition, there are separate dials and selector levers for the speeds and feeds, and knobs for engaging the various traverses, in both

directions of movement.

Special multi-spindle units are provided for boring operations on headstock and gearbox castings that are required in greater numbers, and the equipment for machining a total of 13 holes in hand-feed gearboxes for type 2620A machines is shown in Fig. 11. This jig is used on the small boring machine in the background, and a workpiece



may be seen at the right. All the necessary drills and multi-tooth boring cutters are kept mounted on arbors in the fixture, and the ends of certain arbors may be seen projecting at the left. Each arbor, in turn, is connected to the boring machine spindle by means of a quick-change coupling. High-speed steel drills are employed, and the cutters have tungsten-carbide tipped teeth. The casting is located from the flange and previously machined holes, and when certain of the holes in one plane have been bored, the machine table and the fixture are indexed through 90 deg.,

to enable further operations to be

carried out.

Adjoining the main workshops, there is a well-equipped standards room for checking tools and gauges, and most of the workers in this section are women. Tools and gauges are checked in the workshops each time that they are used, and are sent for inspection in the standards room

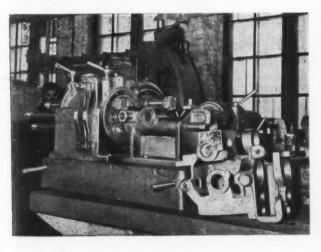
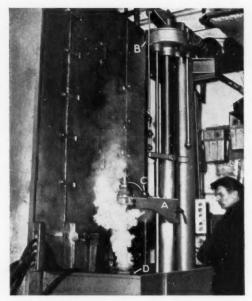


Fig. 11. Hand-feed Gearboxes, One of which is Seen at the Right, are Bored with the Aid of the Large Fixture Shown. The Fixture Incorporates 13 Spindles and Cutting Tools, and is Used on the Small Boring Machine in the Background



at predetermined intervals, based on statistical analysis. There is a heat-treatment department at one side of the light-machining bay, and the equipment includes pit-type furnaces for nitriding treatment, with capacity for workpieces up to 3.5 metres (approximately 11½ ft.). A large high-frequency unit with a rating of 200 kW. is also installed. This unit supplies power for the induction hardening rig, shown in Fig. 12, which provides for the treatment of workpieces up to 450 mm. (17.7 in.) diameter by 900 mm. (35.4 in.) long.

### INDUCTION HARDENING EQUIPMENT

The induction hardening rig has a large tank for quenching oil, above which can be mounted interchangeable ring-type work-coils. A vertical column at one side of the tank supports a vertical guide-member, whereon slides a sleeve carrying a pair of cantilever brackets, one of which may be seen at A. There are two feed-screws parallel with the guide-member, and one of these screws provides for raising and lowering the sleeve and the lower cantilever bracket, which is permanently secured to it. The bracket A incorporates a split bearing, so that it may slide on the sleeve and be clamped to it by means of a lever-screw, and the second feed-screw provides for adjustment of the bracket A, when the clamping screw has been released. Each screw is driven by an individual electric motor, mounted on a platform at the top Fig. 12. Spindles and Shafts are Induction Hardened by Means of this Rig, which is Installed in the Main Heat-treatment Department. The Workpiece is Supported Vertically, and is Lowered Through an Inductor Coil into a Quench Tank

of the column, through the gearbox B. These motors are independently controlled by push-buttons on the pendant panel seen adjacent to the operator in Fig. 12. The sleeve assembly is counterbalanced by a weight in the column, to which it is connected by a steel cable.

At the outer end of the lower cantilever bracket there is a chuck mounted on a vertical spindle which can be motor driven. The bracket A has a semi-circular seating and a screw-operated, swinging clamp at its extremity, these members serving to hold a short quill assembly, with a live cone-centre at its lower end. This centre can be raised and lowered by means of a barrel-cam, to which the handle C is connected. The arrangement is such that shafts and similar workpieces can be passed through the work-coil, indicated at D, and gripped at one end in the jaws of the chuck, when the latter is in its uppermost setting. The other end of the workpiece is then supported by the cone-centre secured to the bracket A. By engaging the chuck-spindle drive, the work is rotated, before the high-frequency supply to the coil is switched on. After a brief dwell period, to allow for the initial heating of the work, the drive to the traverse screws is engaged, and the sleeve, brackets and work are lowered. The workpiece passes through the coil at a suitable traverserate, so that it is heated to the desired depth, and passes into the oil bath whereby it is progressively quenched. As may be observed, a considerable volume of heavy smoke is generated during the induction hardening operation, and, normally, a large sheet-metal shroud, connected to an exhaust system, is swung over the working zone, and the smoke and fumes are extracted. The photograph for Fig. 12 was taken when the shroud was not in position, to enable details of the gearbox and drive arrangements for the traversing screws to be observed.

In addition to serving the rig that has been described, the high-frequency generator also supplies power for another installation in the machine shop adjoining the heat-treatment department. This equipment comprises a Kolomensky lathe, and a large inductor coil assembly, suspended from an overhead rail above the lathe bed. The coil

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Fig. 13. Part of the Main Assembly Shop with the Sub-assembly Bench for Building Hand-feed Gearboxes in the Foreground. When the Assembly Operations have been Completed, the Gearboxes are Transferred to a Bench at the Side of the Machine Assembly Section, in the Background

assembly is enclosed in a split shroud, and incorporates cooling-water sprays. Workpieces, such as spindles and shafts, up to 1 metre (3·28 ft.) diameter by 10 metres (32·8 ft.) long can be mounted in the lathe, and the inductor coil assembly can be coupled to, and traversed by, the lathe saddle. The coil can be adjusted for height relative to the work-surface, and by rotating the work and traversing the coil, workpieces of considerable size can readily be induction hardened.

### MACHINE ASSEMBLY SHOPS

Due to restrictions on factory building, the space available for the assembly of standard and special machines is somewhat restricted, and conditions are rather cramped. The main assembly shop is divided into two bays, both of which are spanned by overhead travelling cranes, and standard boring



machines are built in rows that extend down the length of one bay. Sub-assembly operations are carried out at benches in the adjoining bay, and the bench for the assembly of a given unit is located adjacent to the station in the main assembly bay where that unit is fitted to the machines. A typical sub-assembly bench is shown in Fig. 13, and here hand-feed gearboxes are built. The main castings for these units are bored in the fixture

seen in Fig. 11. Gearboxes are assembled in batches (of ten, in this instance), and, when completed, the batch is transferred to a bench that extends down the side of the main assembly line, seen in the background.

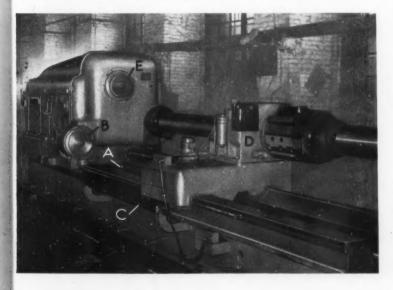


Fig. 14. This Special Boring Unit is One of Three to be Incorporated in an Installation for Machining Electric Motor Frames. The Boring Bar has Provision for Feeding the Cutting Tool Radially

Among the equipment in the assembly section for special-purpose machines was the boring unit seen in Fig. 14. This unit is one of three which will form a special installation for machining the bodies of large electric motors. The headstock is of typical Sverdlov design, and is generally similar to those fitted to the large special-purpose machine in Fig. 6. Driven by a motor of approximately 50 h.p., it has spindle speeds ranging from 16 to 250 r.p.m., a speed of 125 r.p.m. being employed for this particular application. traversed on the vee and flat guideways of the bed by means of a short screw and a long half-nut, part of the latter member just being visible at A between the bed-ways. The travel of the headstock (and the boring bar fitted to the headstock spindle) is indicated by the large rotating dial B. This dial is geared to a vertical shaft, at the lower end of which there is a pinion that meshes with a finepitch rack secured to the front shear of the bed. An indexing stop bar C is also fitted at the front of the bed, and carries adjustable dogs which engage limit switches on the headstock to control

the length of travel, and engage the tool retraction and return motions, when the unit is operating on a semi-automatic cycle. A fixed dog at the far end of the bed serves to stop the head at the end of the return stroke.

The machine is seen fitted with a large boring bar, which incorporates mechanism for feeding the tool radially. This bar is supported in a close-fitting, pressure-lubricated bearing in the steady unit D, and a second outboard steady will be provided to support the free end of the bar. Since the bar must slide and rotate in the steady bearings, it is made from nitriding steel, and hardened to Rockwell 70 C. The bar is of tubular construction, and to facilitate production, it is in two sections, which are coupled together on the side of the cutter head remote from the headstock. Radial adjustment of the tool is effected from the headstock, and the tool movement is indicated by the large dial E.

Further articles in this series, concerned with Soviet engineering plants and research establishments, will be published shortly in MACHINERY. Re

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# Sump Drilling Fixture with Hydraulic Clamping

In the accompanying illustration is shown a set-up—with guards partially removed—employed at the works of Jaguar Cars, Ltd. It is necessary to drill 30 holes of ½ in, diameter through the flange of a steel oil sump, which is 0.048 in. thick, and is backed up by ¼-in. thick stiffening plates, spot welded at intervals. Pressure of the drills against the stiffening plates tends to spring them

away from the flanges, and swarf might enter the gaps thus formed, and cause distortion.

Provision has therefore been made for secure clamping around each hole. For this purpose, 30 Newton hydraulic jacks (Newton & Bennett, Ltd.) are employed, each of which operates a forked clamp. The component is thus lifted ¼ in from the loading rails and held securely against the

drill thrust. At one end, the clamps are carried on a falling gate, which can be locked in position and serves as an end location for the component.

Clamping is controlled by a single hand-operated valve which admits air, at 80 lb. per sq. in. pressure, to two Newton hydro-pneumatic intensifiers, of 10 cu. in. displacement, which are coupled in tandem. A pressure switch is incorporated in the system, and the machine cannot be started if the pressure is below a predetermined value. The floor-to-floor time is less than 2 min.



Drilling Fixture for a Jaguar Car Sump Incorporating 30 Newton Hydraulic Jacks

# Automation Applied to Small-batch Production

Automation, hitherto, has been applied mainly to the quantity production of identical parts. Recently, however, a battery of three numerically-controlled machine tools has been installed in one of the plants of the Hughes Aircraft Co., Culver City, Calif., U.S.A., which can simultaneously handle three different kinds of parts. Moreover, by merely changing tapes and work fixtures, which can be carried out in two or three minutes, other types of work can be handled. Consequently, it may be economical to produce even a single piece on the machines, and in an aircraft plant, for example, it is not necessary to maintain substantial inventories of those parts which are required only



Fig. 2. Digitape Panels for the Electronic Control of All Movements of the Battery of Machines Seen in Fig. 1

occasionally. The machines were built by the Kearney & Trecker Corporation, Milwaukee, Wis.,



Fig. 1. Battery of Tape-controlled Machines for Performing Milling, Drilling, Reaming, Tapping, and Boring or Fly-cutting Operations on Three Different Parts Simultaneously



Fig. 3. Various Workpieces that have been Produced (Three Different Forms Simultaneously) and the Corresponding Control Tapes

and are operated by the Digitape control system, which was developed by the Hughes Co. With this system, equipment is operated from punched tapes and controlled by "transistorized" digital computers.

The line of machines which are shown in Fig. 1 are seen set up for producing parts for the Hughes electronic armament-control systems used on American and Canadian all-weather interceptor aircraft. On the first machine (at the far end) provision is made for performing any number of milling operations on a part, and the second machine can carry out a series of drilling, reaming, tapping, or counterboring operations. The machine in the foreground has two spindles for boring or fly cutting.

Successive operations can be performed at each station as the machines are designed for movement in three directions—in-and-out, up-and-down, and side-to-side. A series of holes or surfaces can thus be machined by any one unit, the machine performing indexing movements to position the cutters in relation to the work. Twenty different tools are accommodated by the turret on the central machine. This turret is indexed automatically to bring any required tool into line with the work.

It may also be noted that the operating radius of the fly cutter on the boring unit can be automatically changed to meet requirements. The work fixtures can be indexed under numerical control to present various faces toward the tools.

Fresh workpieces are loaded on fixtures as they come to the operator at the right-hand end of the line. They are then carried by a chain conveyor to the back of the line, where they are released on to a gravity conveyor that carries the fixtures to the far end of the machine. Here, the fixtures are placed on the transfer mechanism at the front of the machines.

From this point onwards, transfer of the work fixtures from machine to machine and operation of the various members of each machine—as well as indexing of the fixtures—are controlled by tapes in the cabinet seen in the foreground in Fig. 2. Four tapes are provided for this battery of machines to enable them to be set up for handling as many as four different parts. In theory, an unlimited number of tapes could be set up if suitable provisions could be made for handling a considerable variety of parts in sequence. Only three tapes would, of course, be in operation at any one time.

After each machine has performed the specified number of operations on a given part, the fixture and work are automatically transferred to the next



Fig. 4. Plug-in Circuit Boards, of the Type Here Being Inspected, are Employed in the Digitape Control Cabinets

Fig. 5. Machines Arranged to Perform a Series of Operations on Three Different Workpieces Simultaneously Under Tape Control

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unit. This procedure is repeated until the finished part reaches the reloading station. Where the parts are of simple form, more than one can be carried by a single fixture.

To the left of the tape cabinet in Fig. 2 are the cabinets which receive information from the tape "readers" and convert it into instructions for the various machine

movements. The use of printed circuits, transistors, and diodes in the cabinet units saves space and reduces maintenance costs. Tapes are punched by means of a Hughes-designed key-

board. They can be readily produced by a typist who presses keys corresponding to numbers and symbols on a planning sheet prepared by an engineer. By means of the control boards, compensation can be made for tool wear without the need for re-punching tapes. Fig. 3 shows a variety of parts and, with each, the tape provided to carry it through the complete series of operations performed by the three machines. In Fig. 4 an engineer is holding a typical plug-in circuit board from one of the control panels.

Fig. 5 is a close-up view showing various details of the machines. The milling machine in the background can be operated in three directions at feed rates ranging from 1 to 150 in. per min. and the spindle speeds range from 50 to 5,000 r.p.m.

An outboard support is provided for the spindle quills of the drilling machine, as may be seen in Fig. 6, so that special bushing plates are not required. Taps are fed by lead-screws to ensure accurate threading. If a tap or drill is accidentally broken, the spindle retracts. Drill spindle speeds from 110 to 9,000 r.p.m. are available.

The two boring spindles in the foreground of Fig. 5 cover a wide range of hole sizes. One spindle can be adjusted radially while the machine is in operation, and the other is arranged to receive a milling cutter.

Set-up time on the machines has been practically eliminated—in making a work change, all that is normally necessary is to change a tape. Only one operator is required, and he can be readily trained.



Fig. 6. The Turret on the Drilling Unit which Accommodates 20 Different Tools

# Microstics Grinding Arbors

A range of grinding arbors, some examples of which are shown in Fig. 1, has been introduced by Microstics Ltd., 218 Mare Street, London, E.8, for operations on hole bores down to 0.07 in. These arbors are the subject of a patent application.

The standard range covers wheel diameters from ½ in. A feature of the arbors is that the abrasive is not moulded separately and then secured to the shank by cement, but deposited and bonded in position. Normally, the seating portion of the hardened and ground steel arbor is prepared with a slight knurl, but it is stated that a very effective bond can also be obtained on a plain surface. Fig. 2, is a view of a sectioned arbor and the intimate contact between the abrasive and the steel will be observed.

Apart from the standard forms with cylindrical wheels and shanks, special arbors can be supplied to meet particular requirements. Two such arbors are seen in the foreground of Fig. 1, where the abrasive has a concave end surface to provide for simultaneous face and bore grinding. In other instances, the shanks may be of special form to suit the machine spindle mounting arrangements. Such special arbors may be returned to the makers for re-coating when the abrasive has been consumed.

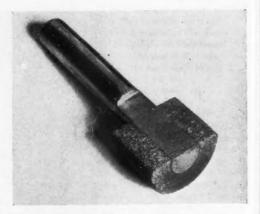


Fig. 2. A Microstics Arbor Sectioned to Show the Intimate Contact Between the Abrasive and the Steel Supporting Portion

With the method of construction employed, it is claimed, the abrasive head is more effectively supported and the maximum thickness of abrasive is provided compatible with arbor strength and outside diameter. Even when the abrasive has worn very thin it will not crack off the supporting shaft during dressing or grinding, and can be used right down to the steel surface. It is stated, indeed, that an arbor may be dropped on a concrete floor without damage.

A special abrasive mixture is employed for these arbors which is necessarily of such a composition that it can be bonded at a temperature that is not detrimental to the metal. This mixture, it is

stated, is suitable for a wide range of precision grinding operations and provides a free cutting action with absence of loading or glazing. It is further claimed that the wheels will operate effectively wet or dry, over a considerable range of speeds, with a minimum of dressing and with a high rate of metal removal.

As an example of the results obtained with these arbors it is reported that 1¼-in. diameter by 1¼-in. long bores in milling cutters of Osborn's S.O.B.V.

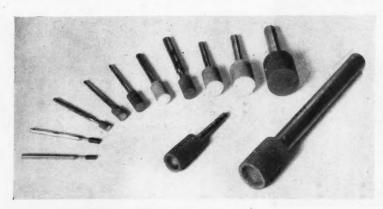


Fig. 1. Standard and Special Arbors Made by Microstics, Ltd. The Abrasive is Moulded and Bonded in Position on the Arbor

10 per cent cobalt alloy were ground dry, with a %-in. wheel, at a speed of 13,000 r.p.m., to limits of -0.0001 +0.001 in. The average metal removal was 0.008 to 0.010 in. and the average number of holes ground per arbor, without attention after the initial dressing, was 66.

In another instance, 76-in. diameter by ½-in. long holes were ground in steel components hardened to 62 Rockwell C, with a ½-in. diameter wheel at a speed of 20,000 r.p.m., to limits of -0.00001 +0.0001 in. Average metal removal was 0.006 in. per 0.001 in. of wheel wear, and 10 holes were ground to a surface finish of 5 micro-inches, at the rate of 1 min. per hole, before the wheel required dressing. The finish obtained in these components was such that a honing operation, required for the method previously employed, was no longer necessary.

As an indication of the performance obtainable on S.80 stainless steel, it is stated that 1½-in. by %-in. long bores were ground wet with a ½-in. wheel running at 60,000 r.p.m. to limits of ±0.0001 in.

Average metal removal was 0.006 in. and wheel wear 0.0002 in. per hole. Twelve holes were finished to 6 micro-inches, and the time per hole was 3½ min. Next, some components of the same design, but in aluminium, were ground to the same limits, at the rate of one in 2 min. Wheel wear was 0.0001 in. per hole, and a finish of 11 micro-inches was obtained. Subsequently, grinding of the stainless-steel components was resumed. The wheel was dressed only before grinding was begun, and during the sequence of operations described it received no attention, and was still not in need of re-dressing at the conclusion of the tests.

A tool-room operation which was carried out on a Moore jig grinder, involved the finishing of 0·202-in. diameter by %-in. long bores with a 0·19-in. wheel. Grinding was performed dry, with a spindle speed of 20,000 r.p.m. Average metal removal was 0·025 in. and 10 holes were completed before the wheel required re-dressing. The amount of wheel wear during this period was 0·002 in.

# A High-precision Lathe Headstock\*

Workers in the Eindhoven Research Laboratories of N. V. Philips Gloeilampenfabrieken, Eindhoven, Netherlands, were faced with the problem of machining flat or profiled end surfaces on such items as plastics lenses to a high degree of accuracy. Although normal and special toolroom

lathes provide for machining accurate cylindrical surfaces to tolerances of a few thousandths of a millimetre, and with surface roughnesses of only a few micro-inches, as a rule these machines are not fitted with spindle thrust bearings which will enable such tolerances to be maintained during a facing or end profiling operation. A spindle bearing which enables a very high degree of axial and



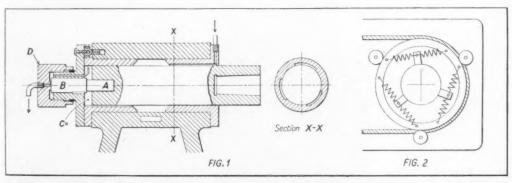


Fig. 1. Sectional View of a Lathe Headstock Spindle Designed by Philips Research Laboratories, Eindhoven, for Precision Facing Operations. Reduced Air Pressure in the Compartment C Causes the Spindle End to be Held in Contact with the Thrust Block B. Fig. 2. The Pulley for Driving the Spindle on the Precision-facing Lathe is Supported on Three Rollers, and the Drive is Transmitted Through Steel Springs



Fig. 3. Photomicrograph, at About 250X Magnification, of the Surface of a Flat Plastics Disc Machined with a Diamond Tool on the Precision Lathe, Showing the Uniform Groove Width from which the Very Low Value for Axial Spindle Movement can be Deduced

radial accuracy to be achieved has been developed in the Laboratories, and a sectional view of a lathe headstock incorporating such bearings is shown in

The cross-sectional form of the bearing employed in this headstock is indicated at the right, and it will be seen that the spindle is supported by three similar equally-spaced surfaces. The bearing is of bronze and the internal supporting surfaces were accurately lapped to size with a tolerance of only 0.001 mm. The steel spindle has been finished to the same tolerance, and the clearance between the two components is such that a drop of 5 deg. C. from the temperature at which the combination is designed to operate, would cause seizure due to the difference in contraction of the two materials. At the rear end, the spindle is fitted with a piece of "improved wood" A, the outer end of which rests against a stationary metal thrust block B, the surface of the latter having been lapped plane and at right angles to the spindle axis to a high degree of accuracy.

The end of the spindle is held in contact with the thrust block with a constant force by means of a suction pipe which maintains a fixed pressure, below that of the atmosphere, in the closed compartment C. Axial adjustment of the thrust block can be effected with the aid of the micrometer sleeve D, and in this way the workpiece can be displaced by extremely small increments in relation to the tool. The low pressure in the compartment C also ensures that the spindle lubricant, which enters the housing at the opposite end, is effectively distributed. This distribution is essential for accurate radial support of the spindle. Problems associated with the close fit of the spindle are avoided by maintaining the bearing at a temperature of 30 deg. C., by means of an electric heating element.

To enable accurate results to be obtained, the transmission of vibration by the spindle drive must be avoided, and a special pulley, details of which are shown in Fig. 2, is therefore employed. This pulley is not mounted on the spindle but is carried on three rollers, equally-spaced round its circumference, and connected to projections on the

spindle by means of springs. As a test of the accuracy obtainable with this equipment, a flat plastics disc was machined with a diamond-tipped tool having a nose-radius of 0.02 mm. (0.0008 in.), which was fed at the rate of 0.0009 mm. (0.00035 in.). A photo-micrograph, at approximately 250 x magnification, of the surface thus produced, is shown in Fig. 3, and the grooves have a width of 0.0009 mm. Close examination of the photograph has shown that the groove width does not vary by more than 5 per cent. It follows that during the 5-sec. machining period, the axial displacement of the lathe spindle relative to the tool was not more than 10 per cent of the groove depth, which, by calculation, is approximately 0.00005 mm. Consequently, the axial displacement did not exceed 0.000005 mm. (0.2 micro-inches).

The lathe was also employed for machining a cavity resonator for 8.75 cm. wavelength, for highprecision measurement of the dielectric losses in solids. In machining this cavity, it was essential that local unevenness of the surfaces should be as small as possible in relation to the depth of penetration of the high frequency currents, which was about 0.001 mm. for the wavelength in question. Measurements of the quality factor of the completed cavity resonator confirmed that the unevenness of the machined surfaces was very small in relation to the penetration depth. Another operation carried out on this lathe is the machining of the aspherical correction plates of mirror cameras for X-ray fluorography.

PUBLIC SERVICE VEHICLE CHASSIS produced during the first three months of this year, including those for trolley-buses, reached a total of 2,626, of which 1,413 were produced for export. For com-

parison, the corresponding figures for the same period last year were 2,343 and 1,317, respectively.

# Some Aspects of Czechoslovak Technical Education

The rapid post-war economic development of Czechoslovakia has necessitated a considerable expansion of the arrangements for technical education, the facilities, it is stated, having been increased sixfold, compared with the pre-war period. Today, technical training is provided for approximately 140,000 young people, and in addition, several tens of thousands of employed men and women study at technical evening schools. There are now more than 400 technical schools, divided into eight main groups, which cover medicine, agriculture, education, and music, for example, as well as the various branches of indus-The latter is served by some 300 schools organized in 17 sections, and 84 of the schools are concerned primarily with engineering.

Boys and girls who have successfully completed studies at the general educational schools up to the age of 14 years, enter the technical schools for a four-year course, at the end of which they must take an examination. The studies are closely connected with practice throughout, and it is stated, for example, that the pupils of an engineering

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Fig. 1. This Girl Student is Undergoing Practical Training at a Czechoslovak Technical School

school in Prague successfully designed refrigerating equipment for goods trains bringing foodstuffs from China. Girls form a proportion of the students in engineering technical schools, where importance is attached to workshop training (Fig. 1).

Tuition at all Czechoslovak schools is free, and students at the technical schools receive a scholarship according to the financial circumstances of the parents. The total sum devoted to this purpose in

the school year 1957/8 is stated to have been 150 million crowns, or £7½ million at the nominal rate of exchang. The majority of the technical schools have hostels attached, at which, for a small fee, the student receives full board and lodging. A technical school with hostel facilities, recently built in Prague, is shown in Fig. 2.



Fig. 2. A Technical School with Hostel Facilities Recently Built in Prague

Before the final examination is taken, the student receives notification from the authorities as to his or her future place of employment, together with details of the wages to be paid, and if the candidate is successful in the examination it is stipulated that he or she must remain in the job selected for at least three years. In this way, a steady flow of technically-trained workers to the various industrial districts is ensured.

The social standing of the student corresponds closely with the social distribution of the population, and in the year 1957/58 about 63 per cent of the students were the children of factory workers or farmers. The average number of students per teacher is 30, and in 1956/57, there were 1,514 students at the technical schools per 100,000 of

the population.

As in the case of the ordinary grade technical schools, the growth of the universities and advanced technical schools of university standing has been very rapid. Whereas, before the war, only nine universities existed in Czechoslovakia,

there are now 40 establishments considered to be of university status. The number of students attending universities and colleges before the war is stated to have been less than 19,000, but now about 80,000 are either attending full time, or are studying in the evening or by correspondence courses. Some 36,000 students are taking technological subjects. University tuition is free, and scholarships are awarded to cover living expenses.

University courses also include a period of practical training in the industry concerned, and diplomas are granted upon the submission of a thesis. The subjects for the latter are carefully chosen in collaboration with the factories, as well as the various scientific and research institutes. It may also be noted that experts with practical experience in industry are chosen as members of the state examination commission which judges the work of the students. Like students from the technical colleges, university graduates are notified of their future places of employment, and the pay they are to receive.

# Tiltman Langley Roller-type Clutch

A clutch of new design, the principle of which is shown by the accompanying perspective drawing, has been introduced by Tiltman Langley, Ltd., Redhill Aerodrome, Surrey. Of small dimensions, this clutch is intended for applications where

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robustness is important, and it will transmit about  $0.5\,\mathrm{h.p.}$  at speeds up to  $1,500\,\mathrm{r.p.m.}$ , depending on the nature of the load. It is stated that it will operate with equal efficiency at temperatures down to  $-40\,\mathrm{deg.}$  C. or under tropical conditions.

As illustrated, the housing A, which is the driving member, rotates in a clockwise direction, and when the control wheel C is held stationary, by the pawl D, it prevents the rollers from being forced into the wedge spaces between the housing and the cam, B. This pawl can be arranged for operation mechanically or by a 7-watt solenoid.

When the pawl is withdrawn, the control wheel is caused to move clockwise, due to the friction of springs interposed between the housing and the cage, the latter being integral with the wheel. As a result, the rollers are moved into engagement with the cam, which is secured to the output gear. Re-engagement of the pawl arrests the control wheel, and the rollers are "kicked" out of engagement.

Clutches can be supplied with various arrangements for mounting the pawl and solenoid, to suit the direction of rotation and installation requirements. There is also a wide choice of standard gears, and special gears can be provided to order.

Perspective 'View Showing the Principle of the Tiltman Langley Roller-type Clutch

# Notsa Engineering New Measuring Room

An important addition to the precision engineering and toolmaking facilities of the Notsa Engineering Co., Ltd., Aston-on-Trent, near Derby, has been made by the establishment of a well-equipped measuring and standards room, which has been granted certificates of approval by the A.I.D. and the Air Registration Board. As well as serving the needs of the company, this development enables a high-class metrology service to be offered to other firms which may be interested.

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Société Genevoise instruments installed include a type MU-214B universal measuring machine which incorporates precision scales and micrometer microscopes reading to 0-00005 in. The measuring range is 16 in. longitudinally, 4 in. transversely, and 6 in. vertically, and among the equipment is a circular dividing table and a goniometric microscope for measuring angles. There is also a Société Genevoise type MUL-250 shop gauge measuring machine, fitted with precision scales and micrometer microscopes, for which a full range of accessories is provided. For making comparative measurements, there is a type MI-6B high-precision micro-indicator, suitable, for example, for the in-

spection of gauge blocks, reference discs plugs, and balls and ball A magniguideways. fication of 10,000 x is provided by optical and mechanical means, and readings to 0.000005 in. are observed on a graduated scale with luminous index which eliminates parallax errors. measuring range is  $\pm 0.00025$  in. and the total plunger travel, 0.08 in. Three different measuring tables, mounted on an indexing turret, readily enable a wide variety of workpieces to be handled. These three instruments are seen in the view of the standards room given in Fig. 1, and it may be noted, that very shortly a Société

Genevoise type MUL-1000 universal measuring machine of 40-in. capacity, will be delivered, together with a type AP-6A profile projector. An OMT toolmakers' microscope, and Sigma mechanical and electrical comparators are in use.

Other important equipment includes a Taylor-Hobson Talyrond Model I roundness measuring machine, and a Talysurf Model 3 surface measuring instrument, which are seen in Fig. 2. On the Talyrond machine, internal and external diameters up to 12 in. can be checked, and workpieces up to 18 in. high are accommodated. An electric displacement indicator, carried on a spindle which is accurate to 0.000003 in, for centre of rotation, is moved round the stationary workpiece, and the signal from the indicator is amplified and fed to a polar co-ordinate recorder whereby straight radial ordinates are marked on an inkless Teledeltos paper chart. Provision is made for suppressing, if desired, the record of closely-spaced irregularities, to enable the general shape of the specimen to be more easily assessed. Conversely, the record of the general errors can be filtered out to facilitate study of the local irregularities. The use of Barrymount

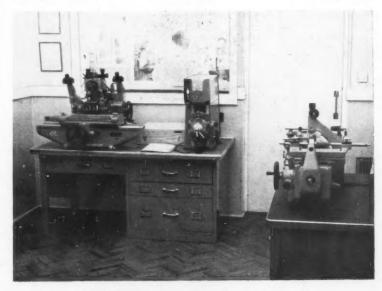


Fig. 1. S.I.P. Precision Measuring Instruments in the New Standards Room of the Notsa Engineering Co., Ltd.

[Cementation (Muffelite) Ltd.] anti-vibration mountings for this Talyrond machine may be noted.

For the Model 3 Talvsurf instrument which is installed, datum and right-angle attachments are provided which considerably increase the range of application. The right-angle attachment enables the pick-up to be mounted at 90 deg. to the normal position so that surface finish measurements can be taken between deep shoulders, as found, for example, on crankshafts. With the datum attachment, profile graphs and average readings of straight and curved surfaces can be obtained with reference to a

datum within the instrument, independently of the

surface under test.

Every effort has been made in the design of this new standards room to ensure the correct conditions for fine measurement. The temperature is maintained at 68 deg. F., within ±1 deg., by a plant installed by Mellor Bromley (Air conditioning), Ltd., Leicester, which incorporates the necessary features of air filtering, humidity control, heating, and refrigeration. The wood block floor is laid on 2 ft. 6 in. of concrete to reduce vibration. Natural lighting is provided by double-glazed windows, and a high standard of uniform artificial

lighting by concealed ceiling fittings.

The facilities to which attention has been drawn are noteworthy in that the Notsa Engineering Co., Ltd., is a relatively small firm, employing about 70 people at the present time. The same policy with regard to high quality and precision is followed by the company in selecting machine tools for production, and the extensive jig boring section is Here, the equipment now worthy of mention. installed comprises a Société Genevoise 2PH and 3K, a Newall No. 2442, a Matrix No. 50, a Hauser IA, a Devlieg 2B36 Jigmil, a 4B72 Jigmil of 48by 72-in. capacity, and two Moore No. 2 grinders. Within the next few months, delivery is expected of several more jig borers, comprising two Newall type 24360P, with optical setting facilities, a Newall Spacematic equipped with the B.T.H. auto-



Fig. 2. Talyrond and Talysurf Instruments in the Notsa Standards Room

matic positioning system, a Société Genevoise 6A Hydroptic, fitted with the D.S.I. automatic positioning system, and a special Société Genevoise Hydroptic No. 7P, with a height capacity under the spindle of 5 ft. 9 in., instead of the normal 39% in. With these additional machines, the company claim they will have one of the largest and best equipped contract jig boring departments in the country, and it is anticipated that the installation of the automatic positioning jig borers will enable them to undertake batch production work of high precision very efficiently.

TECALEMIT QUICK-FIX AIR-LINE COUPLER-A new air-line coupler, known as the Quick-Fix, has been introduced by Tecalemit, Ltd., Plymouth, Devon, to facilitate the connection and disconnection of air-operated equipment from supply lines without waste of compressed air. For coupling, it is only necessary to insert a connector into the coupling unit and press it home. Steel balls, in the coupler, then serve to lock the connector in position to ensure an air-tight joint. Disconnection is effected by sliding an outer sleeve along the body of the coupler to disengage the balls and release the connector. Connectors of this type can be supplied in %-in. 27 t.p.i. and 4-in. 18 t.p.i. sizes. The former are intended for use with air lines, and the latter for fitting direct to Tecalemit Balcrank jet power pumps.

# Peenamatic Shot Peening Machine for Forming Integrally-stiffened Wing Panels

In Fig. 1 is shown one of four Peenamatic travelling-carriage shot peening machines supplied by the Metal Improvement Co., 1721 East 47th Street, Los Angeles, California, U.S.A., to the Wichita plant of the Boeing Airplane Co., for forming integrally-stiffened light-alloy wing panels for aircraft.

Forming is carried out by the impact of 0·174 in. diameter shot which is directed against one side of the wing panel. As a result, the area of the peened surface tends to increase, and the workpiece is caused to bend and assume a convex shape. In this way, forming is carried out without the use of dies, and an important feature of the process is that residual compressive stresses are induced into both sides of the workpiece, with the result that improved resistance to stress corrosion and corrosion fatigue is obtained.

The Peenamatic machine will handle wing panels up to 84 ft. long by 7 ft. wide, with a maximum skin thickness of % in. Forming can be carried out on panels of tapered or irregular plan shape, tapered in thickness, and with various open-

ings. Areas on which shot peening is not to be applied are masked by rubberized tape, as shown.

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Made from ¼-in. thick steel plate, the 96-ft. long work table comprises four sections bolted together, and is inclined at an angle of 30 deg, to the horizontal, so that spent shot is discharged by gravity from the lower edge. Plastics-covered 1½-in. diameter tubes for supporting the work are mounted crosswise on the upper surface of the table at a centre distance of 4 ft. Guide rails secured to the shop floor at both sides of the table support the 12-ft. long peening carriage, which can be traversed at

steplessly-variable speeds ranging from 6 to 60 in. per min. Rapid power traverse at the rate of 40 ft. per min. is also provided. Drive for the traversing motions is taken from motors through reduction gear boxes mounted on the carriage beneath the operator's platform, and thence to a sprocket which engages with a fixed roller chain adjacent to one of the guide rails. Air-operated brakes are incorporated in the drive system. A close-up view of the carriage and part of a formed wing panel is given in Fig. 2.

From the storage hopper mounted on the carriage, the shot is fed by gravity through flexible hoses and gate-type valves, to a total of ten nozzles, adjustably mounted on a carrier which is reciprocated at right angles to the work table, as peening proceeds, by an air cylinder. The shot is propelled on to the work at high velocity by compressed air, which is delivered to the nozzles by way of separate pressure regulators and hand-operated valves. Gauges are fitted to facilitate setting the pressure of air, and, consequently, the peening intensity for each nozzle, independently.



Fig. 1. Peenamatic Travelling Carriage Shot Peening Machine for Forming Integrally-stiffened Wing Panels



Fig. 2. Close-up View of the Peening Carriage of the Machine Shown in Fig. 1, with a Formed Wing Panel in Position on the Worktable. Spent Shot is Returned to the Hopper by Means of a Bucket-type Elevator

Compressed air is delivered to the pressure regulators through a solenoid-operated valve, a moisture trap, and a 2-in. diameter hose which is carried by a reel at the rear, and connected at one end to a swivel joint at a central position. A reel for supporting electric cable, also a dust collecting system are provided, and curtains are attached to both ends of the carriage to prevent the escape of shot to the atmosphere. Spent shot falls from the lower edge of the table on to a motor driven screw conveyor, and is returned to the hopper by way of a bucket-type elevator and a vibrating screen and "air wash" unit.

### Autoset Omni-directional Conveyor Roller

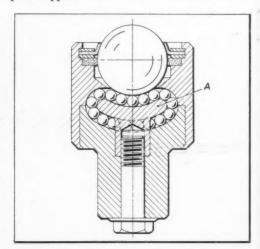
In the figure is shown a sectional view of a recirculating ball assembly recently introduced by Autoset (Production), Ltd., Stour Street, Birmingham 18, for use in ball tables.

The load to be moved is carried by a 1-in. diameter steel ball, which is supported by a number of \$\frac{3}{8}\$-in. diameter balls. The latter can circulate freely in a space between curved recesses in the 2-piece body and the convex and concave upper and lower surfaces of the case-hardened steel central member A. Nylon and felt sealing washers surround the large ball to prevent ingress of dust and dirt to the bearing balls.

As an indication of the very low frictional resistance resulting from this arrangement, it is stated that, for a test carried out by the company, four assemblies were mounted in a framework to support a cast-iron plate carrying a load of 8 cwt. It was then possible easily to move the plate—and with it the load—in any direction by hand, a finger pressure of 2 to 3 lb. only being required.

There are various forms of these assemblies available, including a flat, horizontal plate-fixing type, of 1-ton capacity, a screwed peg-fixing type of 700-lb. capacity, and a further design, which incorporates a nylon pad in place of the recircu-

lating balls and has a rating of 100 lb. In addition, two further types, of 300-lb. and 5-ton capacity, are in the course of design. These omni-directional conveyor roller assemblies are the subject of a patent application.



Sectional View of the Autoset Omni-directional Conveyor Roller Assembly Showing the Main Load-carrying Ball and the Re-circulating Balls which Support it

# Ultra-precision Grinding of Small Cylindrical Parts

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Production grinding of small cylindrical parts to extremely close limits, and the simplified mating of such parts to equally accurate holes, without the need for lapping, are now possible as the result of a long-term research programme carried out in the U.S.A. by Brown & Sharpe engineers. This technique is being applied to the manufacture of accurately-fitting pistons and cylinders for fuelinjection systems, and will offer similar advantages for missile components and other precision work.

These operations are being carried out on Brown & Sharpe No. 5 plain grinding machines—as seen in the heading illustration-which have been refined by means of inspection and carefully controlled building techniques to reduce all alignment to the practical minimum. The machine is equipped with special carbide-tipped centres and an Electralign instrument for electronic alignment of the swivel table. Tempered spring-type mountings protect the machine from external vibrations, and means are provided for filtering the coolant and maintaining it at room temperature. Other features include a rapid traverse arrangement for the wheel-slide, an automatic cycle and sparktiming arrangement, and continuous infeed for plunge-cut grinding. The automatic cycle, sparktiming arrangement is not required, however, if the parts come to the machine round and straight, with carefully lapped centre holes, and only 0.0002 to 0.0003 in. need be removed to bring them to

Other factors contributing to the ultra-precise results obtainable are two recent B. & S. developments, known as Ceda/Size and Electromate. Ceda/Size provides a means of applying and controlling an extremely fine cross-feed, with an electronic-comparator caliper gauge riding on the work (Fig. 1), and an amplifier which registers changes in work diameter in increments of a few millionths of an inch. Wide-spaced graduations of 0-000010 in.



are provided on the amplifier scale so that small changes in work diameter are readily observed. Setting and operation are simple, the procedure being as follows:

1. With the aid of the Electralign, a test piece

is ground straight.

2. A master with the exact mean diameter to which the parts are to be ground, or an accurate sample of the part, is placed between centres.

3. The electronic caliper gauge is applied to the work and with the headstock spindle running and coolant flowing as in actual grinding, the knurled knob at the top of the caliper is adjusted to bring the indicator on the amplifier to zero. The machine is then ready to grind any number of parts on a production basis, size being duplicated within +0.00001 in.

4. In operation, the workpiece is placed in the machine and the electronic caliper gauge is applied. The wheel is advanced to the grinding position, and the work ground until the amplifier indicates that the size is within about 0·000050 in. of zero. At this point, the Ceda/Size lever is depressed, with the result that an extremely fine grinding feed of millionths of an inch per work rev. is applied and controlled. When the indicator on the amplifier reaches zero, the work has been brought to finished size within 0·000010 in. and is round and straight.

An Electromate attachment is combined with Ceda/Size equipment when it is desired to grind pistons for mating with cylinder bores within close clearance limits. The Electromate includes a "computer-selector" unit on which the Ceda/Size

Fig. 1. With the Ceda/Size Method of Producing and Controlling Extremely Fine Cross-feeds, an Electronic-comparator Caliper Gauge Rides on the Workpiece

amplifier is mounted, as seen at the left in Fig. 2, and an auxiliary bore gauge, shown at the right. This gauge can be used to measure bores from

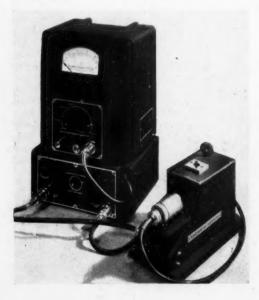
16- to 1-in. diameter.

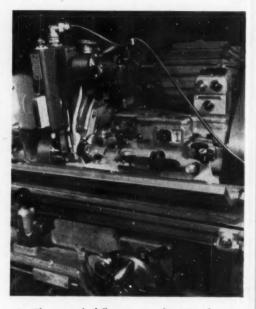
When grinding a piston to mate with a bore, accurate control of the desired clearance can be maintained to  $\pm 0.000020$  in. and these limits can be achieved even when the bores vary by as much as 0.0002 in. on diameter, but the holes must, of course, be straight and round. Wider variations in bore diameter are allowable if clearance limits between piston and bore are greater. For example, if the limits on the clearance are increased to  $\pm 0.00005$  in. then bore variations of as much as 0.0005 in. are permissible.

Selector switches on the computer-selector and amplifier permit exceptional adaptability for all types of precision grinding applications. With these switches, the dial on the amplifier can be arranged to indicate (with any desired increment value from 0.0001 to 0.00001 in.) the following:

1. The diameter of the piece which is being

2. The diameter of a hole in a workpiece on the bore gauge.





3. The actual difference in diameter between a cylindrical piece being ground and the hole in a workpiece on the bore gauge with which the cylindrical piece is to be mated.

Plain cylindrical grinding machines, modified as described, and equipped with Ceda/Size and Electromate attachments, permit semi-skilled operators to:

1. Plunge grind parts to any predetermined size within  $\pm 0.00001$  in.

2. Plunge grind parts to any predetermined fit in a group of mating holes within  $\pm 0.00002$  in., without making individual measurements and calculations, even if the holes vary in size by 0.0002 in.

3. Perform fitting or finishing operations on a group of similar parts, removing as little as 0.00001 in. of stock or up to 0.0002 in. from each piece within an accuracy of  $\pm 9.00001$  in. Once the set-up has been made, the amount of stock removed from each part can be varied within the above limits depending upon individual requirements

4. Take a part from the machine, measure it, replace it in the machine, and remove as little as 0.000010 in.

Fig. 2. The Electromate Attachment for Grinding Pistons to Mate with Bores Comprises a Computerselector Unit and an Auxiliary Bore Gauge

## Kendall & Gent 300-ton Plano-milling Machine

Fig. 1 shows the largest of three plano-milling machines which have been supplied to the Larne works of the British Thomson-Houston Co., Ltd., by Kendall & Gent, Ltd., Gorton, Manchester. It is being employed for machining large turboalternator parts and has a capacity for work up to 29 ft. 9 in. long, by 12 ft. wide, and 8 ft. 6 in. high. There are two vertical milling heads, and provision has been made for fitting a horizontal milling head, if required. In addition, an Asquith drilling and boring head is mounted at the rear of the cross-slide, so that milling, drilling and boring operations on the large workpieces can be carried out with a minimum of handling. Fig. 2 is a side view of the machine.

A description of one of the two machines previously supplied, each of which has a capacity of 18 by 6 by 6 ft., was published in MACHINERY,

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Weighing approximately 52 tons, the table is T-slotted, and a trough which surrounds the working surface collects the coolant for return to the tank. It has a total traverse of 31 ft. 6 in., and is 29 ft. 9 in. long, exclusive of the troughs, and 12 ft. wide overall. The rear end of the table has been prepared so that another table can be coupled to it to provide a tandem arrangement at

some future date. This modification would necessitate lengthening the bed, and the extra lengths would be inserted between the exist-

ing bed joints.

Drive to the table is taken from a 30-h.p. motor with steplessly-variable speeds from 600 to 1,800 r.p.m. The motor is connected by flexible coupling and worm reduction to the gearbox, whence motion is transmitted by two long worms, set to eliminate backlash.

which engage with semi-circular racks secured to the under-side of the table, end pressure in each direction being taken on heavy ball thrust washers. By means of the gearbox and motor speed variation, an overall range of feeds from ½ to 24 in. per min. can be obtained. When rapid power traverse is engaged, the motor operates at maximum speed only to give a rate of 15 ft. per min.

Electro-magnetic clutches are incorporated in the table feed-box to enable the feed or rapid traverse to be selected by push-button at the control desk or pendant. When the feed button is pressed, the appropriate clutch is engaged and the traverse motor is started simultaneously to move the table in the required direction, and at the predetermined feed rate. If the rapid traverse button is then depressed, the table is automatically speeded up to the constant rapid traverse rate.

Electric locking is provided for the table, and safety devices prevent the table traverse motor being started if the table is locked, or the spindle of the boring head being rotated if the table is not locked. As the combined weight of table and workpiece may amount to 80 tons, hydraulic assistance is provided for the hand motion.

Each milling head is driven by a 60-h.p. variable-speed motor, mounted on top of the head,

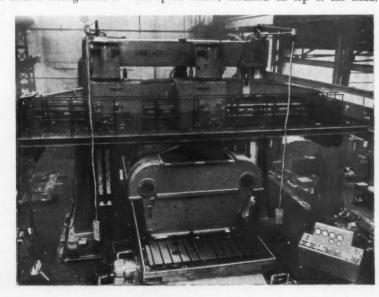


Fig. 1. Kendall & Gent 29½ by 12 by 8½ ft. Plano-milling Machine

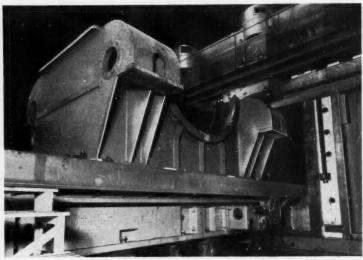


Fig. 2. Right-hand Side View of the Large Kendall & Gent Planomilling Machine

which, in conjunction with a gearbox, provides steplessly-variable spindle speeds, in four ranges, from 6 to 220 r.p.m. The spindles, which have 6-in. diameter driving portions, are of high-tensile steel, and run in ball and roller bearings mounted in large-diameter densified iron sleeves. Each spindle nose has a 15-in. diameter flange, with driving keys, to receive large-diameter face milling cutters. A fine micrometer hand adjustment is provided for each sleeve, also power traverse, at 12 in. per min., by means of an independent 5-h.p. motor.

The milling head feed and rapid traverse motions are obtained in a manner similar to that described in connection with the table, drive being taken from a 15-h.p. steplessly-variable-speed motor, through a feed-box at the right-hand end of the cross-slide. Feeds range from ½ to 24 in. per min., and the rapid traverse rate is 5 ft. per min. Magnetic clutches, again, provide for the selection of feed or rapid traverse.

With an overall length of 36 ft., and a depth of 6 ft. 4 in., the cross-rail, with the milling and boring heads, weighs approximately 54 tons, and is partially balanced to facilitate elevation, which is effected by means of a 40-h.p. motor, at 15 in. per min. Should the cross-slide get out of alignment, owing to uneven wear of the elevating screws and nuts, a compensating clutch, incorporated in the elevating motion, provides means for correction.

When taking a cut, the cross-slide is locked in position by a 1-h.p. electric motor which drives a screw through worm gearing. Lights on the control desk indicate whether the cross-slide is locked or unlocked. In the former condition, electrical interlocks make it impossible for the elevating motor to be started.

Should the spindle motors be overloaded due to excessive depth of cut or feed rate, the table traversing motor or milling head traversing motor, whichever is in

operation, is automatically slowed down. If the overload still persists when the motor has reached its lowest speed, it is stopped. This arrangement protects both the machine and expensive milling cutters.

In addition to push-buttons, the control desk is equipped with ammeters, reversing switches for the spindle motors, and large tachometer dials on which the actual feed traverse rates of the table and milling heads are registered. For use when close scrutiny of the work is necessary during cutting, two pendant push-button stations are provided, with buttons for all traverses.

The approximate weight of the machine is 300 tons, and the width between the uprights is 14 ft. 6 in.

Production of Uranium Fuel Pellets. At the Blairsville, U.S.A., plant of the Westinghouse Electric Corporation, large numbers of fuel pellets for atomic reactors are being produced from uranium oxide power. This powder is mixed with organic binders and is formed into small cylinders on an automatic press, which is enclosed by a plastics shield. Subsequently, the pellets are sintered to eliminate the organic constituents and obtain the required strength. As a considerable degree of dimensional accuracy is required, the sintered pellets are finished by grinding and are subsequently checked for length and diameter.

Finally, the pellets are packed in stainless-steel tubes, in which they are a close fit, and the tube ends are sealed by welding.

# Investigation of Chatter on Radial Drilling Machines

By W. BYE, B.Sc.

Chatter in machining operations is most readily avoided by care in the original design of machine tools. The problem is complicated, however, owing to the increasing speeds and feed rates now required, and the diversity of conditions under which many machine tools must operate effectively.

In modern machine tools, the natural frequencies of individual components are invariably well outside those encountered in service. However, as individual parts are combined in assemblies, the composite natural frequency inevitably falls. A cutting tool, moreover, must normally be mounted on a spindle or slide with the edge unsupported except by contact with the workpiece. In consequence, the assembly incorporating the tool normally has the lowest natural frequency of any part of the machine.

Dr. D. F. Galloway has reported that with the arm of a particular radial drilling machine at the

top of the column and the drill head at the outer end of the arm, resonance could be excited by vibrating the drill head in a vertical direction at a frequency of only 9.9 cycles per sec., and such a low natural frequency is by no means excep-The peak-to-peak amplitude of this vibration was 0.049 in. with an exciting force of only 20 lb. r.m.s., and the potentially serious effect of chatter on both accuracy and surface finish were thus clearly demonstrated. The importance of minimizing overhang was shown by the fact that the peak-to-peak amplitude of resonance was reduced to 0.00018 in. when the radial arm was lowered by 23 in., and the drill head moved towards the column through a similar distance.

#### INDUCTION OF RESONANCE

The latent state of resonance only mainfests itself when it is excited by some vibratory force at the critical frequency. Fig. 1 shows the rapidly diminishing effect as the frequency of the exciting force diverges from the natural frequency of the vibrating system. Should the two frequencies be dangerously close together, it is possible to separate them by changing either the exciting frequency or the natural frequency of the appropriate portion of the machine tool.

Dr. S. A. Tobias and Prof. W. Fishwick² have done much to clarify the factors involved in adopting either of these two courses in connection with drilling operations. In many vibration problems outside the machine tool field, it is simple to vary the exciting frequency by changing the speed of the driving motor. When chatter is being excited as a result of vibration at the speed of the motor or of the transmission gearing, this course is also open to the machine tool designer. The above authors have, however, shown that the, in most instances, chatter, particularly at low frequencies, is induced as a result of vibration generated directly by machining.

In drilling operations, for example, discontinuity in the workpiece may result in variations in the rate of metal removal and in the effective rake angle. By reason of such a disturbance in drilling conditions, a time-dependent component may be



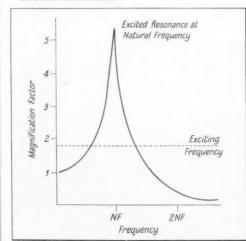


Fig. 1. Magnification Factor Plotted Against Frequency for a Simple Vibrating System. The Sharp Peak Indicates the Powerful Effect of Resonance Even when, as Indicated by the Dotted Line, there is Moderate Damping (Adapted from Galloway)

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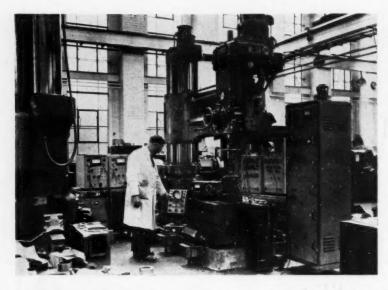
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Vibration Testing, Showing the Vibration Generator with its Power Source and Control Panel, Vibration Meter and Analyser, and Cathode Ray Oscilloscope for Checking Waveforms

Fig. 2. General View of an Archdale Radial Driling Machine Set up for

superimposed on the normal constant thrust.

If the conditions are favourable to vibration, chatter induced in this way will become self-sustaining. For such favourable conditions to exist, there must be a specific relationship between the speed and feed in use, the natural frequency of the vibrating system, the effective damping coefficient of the machine, the thrust characteristics of the drill, and the machinability of the workpiece. The avoidance of chatter, therefore, depends on the elimination of any undesirable coincidence between these six factors.

For convenience, the implications will be confined in the following discussion solely to the important operation of drilling.

#### **ACTION BY MACHINE BUILDERS**

Progressive machine tool makers are concentrating more and more attention on the problem of chatter, partly on account of the increased speeds and feeds to which reference has already been made, but also because production engineers are now required to machine metals which would have been considered "unmachinable" only a few years ago. It must also be borne in mind that many machine tools which are being put into service today will still be in use in ten years' time.

Since drilling has been taken as an example, the procedure adopted, for the solution of this problem, by James Archdale & Co., Ltd., at their Worcester factory, will be considered. Research in this field is under the direction of Dr. Tobias.

whose work on this subject has already been mentioned.

Broadly speaking, vibration testing is carried out by two complementary methods. With the first, machines are subjected to artificial loads, such as the simu-

lation of drill thrust by means of an electromagnetic vibration generator, as shown in Fig. 2. The second method involves measurement of vibration at various points on the machine while drilling is carried out under closely-controlled conditions. Comparison of vibration readings obtained in both types of test enables spurious effects to be eliminated, and it is then possible to correlate vibrator testing unambiguously with normal working practice.

One of the main advantages gained with artificially-induced vibration is that any effects noted during drilling can be greatly magnified to permit study in greater detail.

#### **VIBRATION GENERATORS**

The vibration generator employed for this work is the Model 790 from the range supplied by Goodmans Industries, Ltd., Axiom Works, Wembley. It incorporates a heavy pot-shaped magnet assembly for producing the magnetic field in which a moving coil operates. The armature is a light structure which is suspended inside the heavy pot by means of two spiders, and can move freely in an axial direction, while radial deflection is prevented. Vibration is generated by supplying a sinusoidal current to the moving coil which forms an integral part of the armature. Due to the low axial restraint of the spiders, the armature describes a purely sinusoidal vibrațion at a frequency equal to that of the alternating current fed into it. The vibratory force generated in this way is directly

Fig. 3. The Power Source and Controls for the Vibration Generator are Housed in the Cabinet to the Right of the Operator. Here the Generator is Mounted on the Table to Apply a Horizontal Vibratory Force on a Vertical Milling Machine

proportional to the magnitude of the applied current.

For convenience, the current supply is taken from a valve oscillator, and a suitable heavyduty unit can be seen to the right of the operator in Fig. 3. (This oscillator is an early model, and the latest

version, known as the Type D120, is much more compact.) A knob, which is set with reference to a calibrated dial, controls the output frequency of the signal supplied to the vibration generator. Once this frequency has been set, it remains constant, irrespective of fluctuations of the mains supply or any other variable factor.

The current supplied by the oscillator to the generator can be varied by altering the gain, and once a setting has been made, the value, which is indicated on a sensitive meter, remains constant. Since the "force factor" of the generator (in lb. per amp.) is known, this meter can be calibrated in force, should this be desired.

The facility for varying the magnitude and frequency of the exciting force independently is important. It enables the force to be maintained at a constant value while the frequency is varied, in a few seconds, over the entire range.

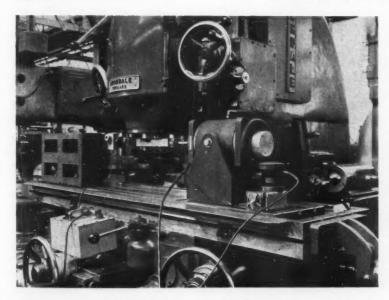


Fig. 4. A Close up of the Goodmans 790 Vibration Generator Adjusted to Apply a Horizontal Oscillatory Attention is Force. Drawn to the Use of a Magnetic Chuck to Hold the Pick-up for the Vibration Meter in Contact with the Machine Table

#### VIBRATION MEASUREMENT

For measuring the resultant vibration, a meter is employed which is connected to an inertia-type crystal pick-up by means of a flexible cable. The pick-up is mounted at any desired point on the machine, and the meter can be placed in any position convenient for the operator. Although the pick-up can be pressed into contact with the vibrating surface if only a single reading is to be taken, it is generally desirable to attach it positively, but temporarily, to the surface either magnetically, as seen in Fig. 4, or by means of a simple screwed mounting point (Fig. 5). With either method, the pick-up can be changed rapidly from the vertical to the horizontal position and is always presented in the same way to the surface, which is important if close repeatability is desirable.

#### MODES OF VIBRATION

Vibration of several radial drilling machines by the method shown in Fig. 2 has disclosed that they have two vertical modes and a number of hori-

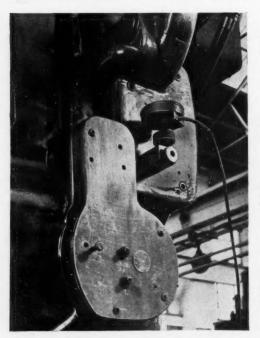


Fig. 5. A Simple Mounting Point for the Pick-up of the Vibration Meter. The Two Screwed Plugs Enable the Pick-up to be Changed Rapidly from the Horizontal to the Vertical Direction

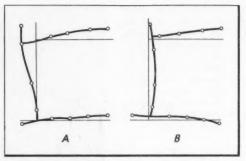


Fig. 6. There are Normally Two Vertical Modes of Vibration for a Radial Drilling Machine, Namely (a) the "Rocking Mode" and (b) the "Tuning-fork Mode." Experience has Shown that Chatter on Such Machines is Associated Purely with the Rocking Mode

zontal modes. Experience suggests that this may be generally true for this type of machine.

The vertical modes, designated "rocking" and "tuning-fork," are indicated diagrammatically at A and B, respectively, in Fig. 6. The thin full lines in these illustrations (which represent the top surface of the arm, the centre of the column and the bottom of the base) are the datum lines for measurement. Readings have shown that these members deform under vibration, as indicated by the heavy lines. The actual amplitude of vibration is indicated by the distance of the circles from the datum line. For clarity, only one extreme position has been shown in each instance, the second being a mirror image on the other side of the datum line.

A typical resonance curve obtained by this method on a particular radial drill is shown in Fig. 7, the ordinates representing relative amplitude between the box table and the drilling spindle. The rocking mode of vibration associated with the sharp peak at 10.2 cycles per sec. can be shown to have a dynamic amplification factor of 14.5, whereas the flatter peak at 26 cycles per sec. (associated with the tuning fork mode) has an amplification factor of only 3.7. This substantial difference in the attenuation of the two peaks is reflected in a marked difference in the vibration in the two modes. The vertical rocking mode has an amplitude of more than 0.005 in. at resonance, whereas the amplitude for the tuning fork mode is less than a tenth of that value.

Although a number of different modes of vibration is theoretically possible in both the horizontal and vertical directions, it by no means follows that

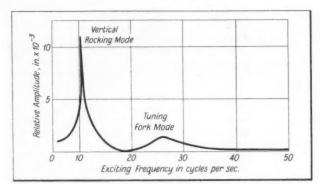


Fig. 7. Resonance Curve for a Typical Radial Drilling Machine which [was Obtained by Vibrating Vertically with an Exciting Force [of 20 lb. r.m.s. The Peaks Associated with the Rocking Mode and the Tuning Fork Mode (Fig. 6) can be Observed

all will be excited in practice. In particular, the radial damping exerted by the workpiece on the drill may be expected to suppress horizontal modes of vibration. Besearch shows that this deduction is correct and that horizontal vibration is of strictly limited importance when drilling. Since drilling tends to have the effect of separating the arm and the baseplate of a radial drill, it was originally supposed that the tuning-fork mode would mainly be excited in service. Experiments with drills ranging from ¼ to 1 in. diameter indicated that this supposition is incorrect, and that the vertical rocking mode is exclusively excited within the range of conditions studied.

#### PREVENTING CHATTER

On the basis of data obtained from such tests, it may be advisable to increase the dynamic stiffness of the structure so as to raise the natural frequency at which resonance takes place. For this purpose it is essential to know the extent to which different parts of the structure of the drilling machine are deformed. It is obvious that no increase in stiffness in undeformed parts can have any beneficial effect. On the contrary, by adding mass at inessential points, the ratio of stiffness to mass can be changed in such a way as to lower the natural frequency and thus to increase the incidence of chatter.

Conclusions can also be drawn from such tests concerning the possible steps which can be taken to avoid an undesirable correlation of the factors controlling chatter. Fig. 8 shows in graphical form the unstable (shaded) and stable (unshaded) regions for the radial drilling machine to which

the curve in Fig. 7 relates. Another unstable region, associated with the tuning fork mode, is located to the top right of the diagram, and is innocuous. This type of diagram is characteristic of radial drilling machines, although the individual shape and detail will vary considerably, depending on the design of particular machines and the drilling conditions.

Since chatter will tend to occur whenever the operating conditions of the machine lie in the shaded area, it is possible to establish various arrangements which will prevent chatter from arising in a particular machine. For instance, if the value of  $Q_e$  (critical damping/2 × effective damping) for the mode of vibration is less than 12, the locus for  $Q_e$  will never intersect

the unstable area at any drill speed. Operation will thus be stable under all conditions and chatter will never occur. In practice, the true

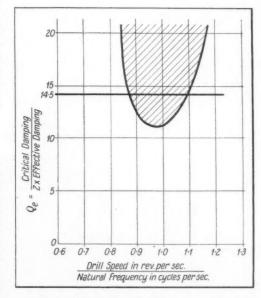


Fig. 8. Typical Stability Chart for a Radial Drilling Machine with the Vibration Characteristics Shown in Fig. 7. The Line for Q = 14·5—representative of the Rocking Mode—Intersects the Curve Indicating Instability in the Rocking Mode for Abscissae between 0·87 and 1·1 (i.e., for Speeds Between 530 and 675 r.p.m.)

value of the effective dynamic amplification factor (Oe) is difficult to compute. For general purposes, however, it is sufficiently accurate to assume that it is equal to the dynamic amplification factor (Q) of 14.5, which can be calculated directly from Fig. 7. Accordingly, a horizontal line is drawn through this value to pass through the unstable curve for values of drill speed from 530 to 675 r.p.m. Confirmation of the essential correctness of the method was obtained from the fact that chatter was self-propagating over the entire band when the practical conditions were made to simulate those used in the construction of Fig. 8.

#### CONCLUSIONS

It is now possible to predict, within fairly close limits, whether a drill will cause chatter under a given set of conditions. This knowledge is of value in that it enables conditions liable to cause chatter to be avoided. Of more fundamental importance is the advance warning given to designers of the effects of proposed constructional changes. Practical drilling tests are important guides to future action, but they supply data only for the conditions actually reproduced under test. The great value of simulated tests with a vibration generator replacing the drill is that the entire range of working frequencies ever likely to be encountered in practice can be investigated in a very short time. It is impossible to leave an unexplored gap through inadvertently failing to visualize particular con-

ditions to which the machine will be subjected.

The method of simulated testing described above is not confined to radial drilling machines. It is a universal method applicable to all machine tools. For instance, Fig. 3 and 4 show vibration generators mounted on a vertical milling machine, and similar methods of testing can be applied to a lathe or grinding machine.

<sup>1</sup> D. F. Galloway, B.Sc. (Eng.), Ph.D., Wh.Sc., M.I.Mech.E., M.I.Prod.E., in a paper "Some Experiments on the Deflections and Vibrations of Drilling Machines" read before the Institution of Mechanical Engineers.

<sup>a</sup> S. A. Tobias, D.Sc., Ph.D., and Prof. W. Fishwick, Ph.D., in a paper "Vibrations of Radial Drilling Machines under Test and Working Conditions" read before the Institution of Mechanical Engineers.

#### Stack-A-Jack Clamp Supports

The Stack-A-Jack packing pieces for machine clamps, recently placed on the market by T. Cowley, 116 Coleman Court, Kimber Road, London, S.W.18, are available in sets, each comprising 80 items, which are housed in a wood case with a plastics insert, as shown in the figure.

Presented in this manner, the various items, which are accommodated in pockets in the insert, can be quickly selected with reference to a chart on the lid, and assembled to provide a maximum of four packing pieces with heights ranging from to 432 in, in 32-in. steps. An example of a packing piece which has been built up from a number of items is seen in the foreground.

The set comprises 14-in. diameter by 7%-in. thick base members, and %-in. diameter "stem" and 'cap" pieces, the former having lengths, over the contact surfaces, of 1/2, 1, and 2 in., and the latter, thicknesses ranging from 1/8 to 1/2 in. Made from steel, case hardened and cadmium plated, the

items are knurled, to facilitate handling, and when assembled they are located in relation to each other by mating spigot portions and recesses. Since the various parts are held to limits of  $\pm 0.002$  in. for length over the contact faces, they may be used. if desired, for supporting stepped

The equipment is also available in sets comprising 40 items, which enable a maximum of two packing pieces up to 431 in. high to be built up. Alternatively, the pieces can be supplied in the requisite numbers without a case, and storage facilities. are then provided by the user.



## Large Milling Cutters Designed for Ease of Maintenance and Setting

If sufficient thought is given to possible maintenance problems during the tool design stage, most of the problems can be anticipated and minimized. However, if maintenance is not considered during design, savings that are expected to result from the use of the new tooling equip-

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As an example, it may be noted that large-diameter face-milling cutters which were designed by the Wesson Co. for installation on an aluminium-billet scalping machine developed by the Consolidated Machine Tool Division, Farrel-Birmingham Co., Inc., have enabled blade grinding time to be reduced to only a few hours, whereas formerly three weeks was required. Because the blades are pre-set, set-up time has been reduced to 45 min. in contrast to the 12 to 15 hours formerly needed. In addition, gauges and setting fixtures, valued at 13,000 dollars, that were originally employed, are no longer necessary.

The scalping machine was designed specially to reduce the time required to prepare rough aluminium billets so that they can be cold-rolled into sheet, strip, and foil. A conventional machine has a single cutter, and each billet must be passed across it twice. Floor-to-floor scalping time on

such machines is between 8 and 10 min., depending on the billet size. Moreover, handling of the billet between passes frequently resulted in scratches on the finished surfaces, which had to be removed by further milling. If such scratches go undetected, long blemishes appear in the finished material, and in either event, such damage is costly.

On the new duplex scalping machine, both sides of the billet are milled at the same time in a floor-to-floor time of about 90 sec. Average stock removal rate is 5,000 cu. in. of aluminium per minute. The first of these scalpers has been installed at the Ravenswood, W.Va., U.S.A., plant of Kaiser Aluminum & Chemical Co. The blades of the cutters rotate at a surface speed of 11,800 ft. per min., and act like fan blades inside the shrouds. A strong down-draught is thus generated, which throws the chips on to a conveyor in a pit below the machine.

Stock removal rates are adjustable by changes in the billet feed rate or the depth of cut, or both. Depths of cut may be as much as % in. on billets ranging in size from 8 to 16 in. thick, 30 to 54 in. wide, and 6 to 14 ft. long. Much power is required to remove chips at a rate of about 1 ton in

4 min. Each cutter is bolted to a direct-drive spindle powered by a 1,000 - h.p., 600 - r.p.m. electric motor. Jordon-type couplings are used so that the cutter heads can be adjusted longitudinally, either independently or simultaneously. The total travel for each cutter head is 17 in., and

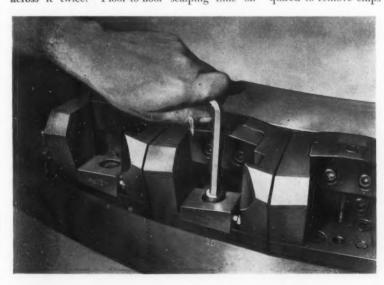


Fig. 1. With the Back Wedges Secured to the Individual Tool-blocks, the Lower Wedges are Positioned and Locked in Place by Bolts



Fig. 2. Each Blade Holder is Retained in the Tool-block by Means of a Single Wedge that Exerts Force in Three Directions Simultaneously

adjustments can be made from the main console in increments of 0.01 in.

#### **CUTTER DESIGN**

Each of the cutters designed for this billet scalper weighs about 2 tons and has an effective diameter of 75 in., and it is believed that they are the largest pre-set, carbide-blade, face-milling cutters ever made. Each cutter has 44 Wessonmetal solid-carbide roughing blades and two solid-carbide finishing blades.

A segmented design was adopted to permit the very substantial savings in maintenance time. Blades are ground after removal from the cutter body, but they can be quickly and accurately re-assembled. Each cutter comprises a solid-steel body ring to which 44 hardened steel blocks are bolted. Each block is located angularly by means of two dowel pins, and identical, removable blade holders are fitted to the blocks.

Incorporated in each block are two tapered wedges for radial and axial adjustment of the blade holder. These wedges need to be set only once during the life of the cutter. Also, once the wedges have been positioned, any holder will be correctly located as soon as it is inserted, and locked.

Outside diameter location of the cutting edges is achieved by adjusting back wedges in the tool-

blocks. The height of the cutting edges is adjusted by lower wedges, which are correctly set in the blocks by means of a master holder. In Fig. 1, one of the lower wedges is seen being locked in place with a bolt. In this illustration, the back wedges are shown secured to the tool-blocks.

Each blade holder has a tapered slot that holds the solid carbide blade with high, positive radial-and axial-rake angles. The holder in each block is secured by a single self-actuating wedge, seen in Fig. 2, which exerts locking forces in three directions at the same time. Each of these units is actually an assembly of a wedge and a bolt. When the bolt is turned clockwise, the wedge is drawn down to tighten the assembly; and when it is turned counterclockwise, the wedge is loosened.

#### HOLDERS DETERMINE CUTTING ANGLES

The design of the holder is the key to the important reductions in grinding and set-up times. Incorporated in each holder are the angles that ensure the required clearance for the blade when the unit is inserted in the block. Only a simple gauging set-up, illustrated in Fig. 3, is needed. Two dial indicators are used—one for checking the distance of the cutting edges from the centre of the cutter body within 0·001 in., and the other

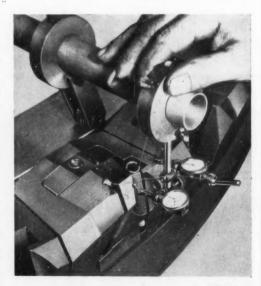
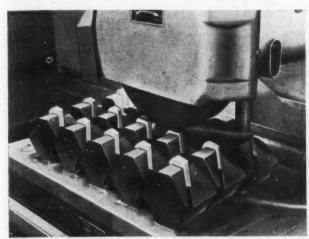


Fig. 3. One Indicator is Used to Check the Distances of the Cutting Edges from the Centre of the Cutter, and the Other to Check the Heights of the Blanks



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Fig. 4. Resharpening Carbide Blades for the Large Face-milling Cutters is Simplified by Using the Blade Holders as Fixtures on a Surface Grinding Machine

for the height, which is maintained within 0.003 in. The indicator support arm is provided with a ball-bearing, roller type steady-rest which bears on the cutter body.

Since the compound angles required on the blade are actually determined by the holder, the latter can be used as the blade-grinding fixtures during resharpening. Consequently, the complicated angles can be ground on an ordinary surface grinder, as seen in Fig. 4. It is only necessary to remove the blade holders from their blocks on the cutter ring, position them on a magnetic chuck, and grind until all the blades have been sharpened.

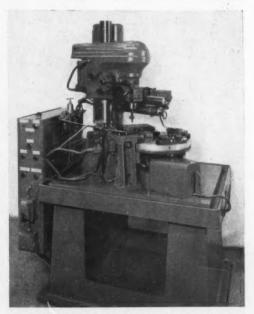
Complete sets of right- or left-hand blades can be ground at one machine loading, and, if necessary, right- and left-hand blades can be ground in mixed loads. As many holders can be mounted on the surface-grinding machine as the magnetic chuck will hold, and relocation in the cutter is a simple matter.

## Pacera Automatic Machine for Chamfering Ring-shaped Parts

W. J. Meddings, Ltd., 16 Berkeley Street, London, W.1, have recently supplied the Pacera automatic drilling machine, here shown, to a German firm, for chamfering at one side only, the bores of ring-shaped parts.

The 4-station indexing table carries fixtures fitted with V-shaped jaws, which are automatically closed for gripping the work by the action of an air cylinder. Next, the table is indexed to bring the part to the working position, and is located, positively, while chamfering is being carried out. During this operation, the drill spindle is controlled by a Pacera-Maxam airhydraulic feed unit, and coolant is delivered to the work in mist form. When the table has again been indexed, after the chamfering operation, the work is automatically ejected from the fixture. At the fourth station, swarf is removed from the fixture by compressed air. With this arrangement, a component may be loaded while other parts are being chamfered and ejected.

Electrical equipment and solenoid-operated air valves for controlling the working cycle, are housed in a separate floor-mounted cabinet. Provision is made for setting the machine by hand.

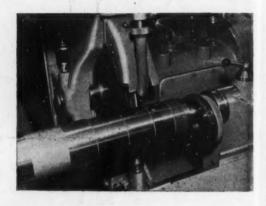


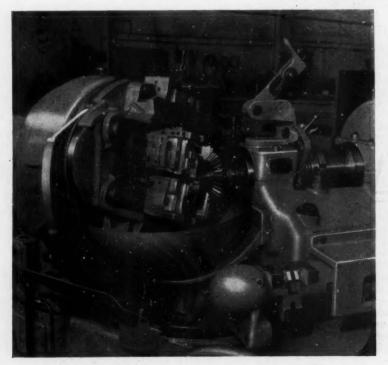
Pacera Automatic Machine for Chamfering Ringshaped Parts

## Round the Shops

#### Some Typical Operations at the Minganti Works, Bologna, Italy

This Lindner (Stedall Machine Tool Co.) grinding machine is employed for all the important threads on such components as spindles for Minganti machines. It is shown set up for operations on the main spindle for the type I/AP turret lathe, which has a 3-in. bore, and two ground threads at one end. The threaded portion in front of the grinding wheel is of 2-mm. pitch, 60-deg. metric form. It has an outside diameter of 105 mm. and is 30 mm. long. This thread accommodates the spindle bearing adjustment nut in the final assembly





Practical tests carried out on Minganti bevel gear generating machines include the cutting of a sample gear. A DCM-306 machine is here shown set up for cutting a 45-deg. test gear of 140 mm. pitch diameter, with 28 teeth of module 5 and 20-deg. pressure angle. At the roughing operation illustrated, each tooth is cut in a period of 18 sec. The machine will cut gears up to module 8 with a maximum tooth length of 90 mm., and gear sets with ratios from 1:1 to 10:1 may be produced. The agents in this country for Minganti machines are Cyril Adams & Co. (Special Projects), Ltd., 70-74 City Road, London, E.C.I.

### with a Camera

For milling the end faces of beds for Minganti T35 turret lathes, two castings are set up, as shown, on a Giddings & Lewis (Rockwell Machine Tool Co., Ltd.) horizontal boring machine. The II-8-in. diameter Coromant cutter has 16 inserted carbide-tipped blades and is driven at a surface speed of 285 ft. per min. A feed rate of 6.5 in. per min. is employed, and for the roughing operation the depth of cut is 0.2 in. The spindle head is fed vertically and only two passes are required to machine the entire end surface of each casting

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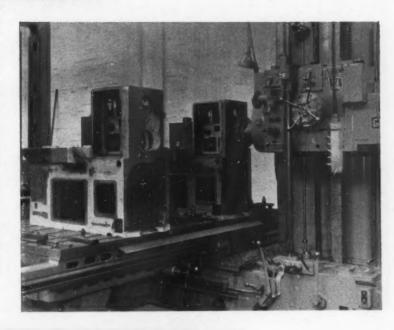
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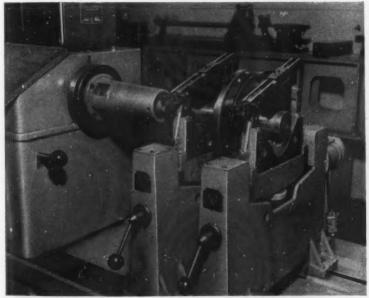
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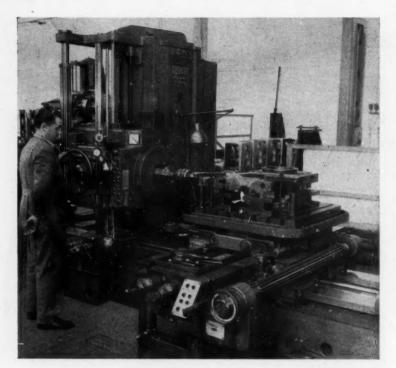
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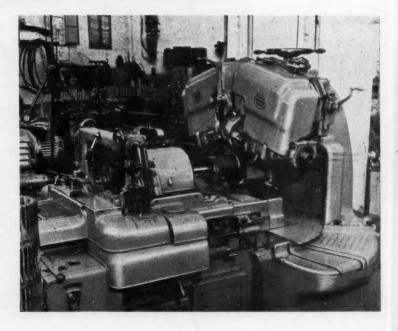


This Schenck (W. & T. Avery, Ltd.) dynamic balancing machine is employed for most of the spindle assemblies for turret and other lathes made by Minganti. Prior to assembly on the spindles, such parts as roller bearings, gears, and clutch sub-assemblies are separately balanced to reduce the amount of correction finally required. Here, part of a headstock spindle magnetic clutch is shown set-up for balancing. A lathe of the 80/100 series incorporates seven of these clutches for obtaining spindle speeds from 80 to 1,500 r.p.m., and six for feed changes



The set-up on a Ceruti Alematic ALF80 [Drummond-Asquith (Sales), Ltd.] machine is for a series of finish-boring operations on a turret lathe saddle, which has previously been jigdrilled. For boring the housing for the automatic feed mechanism, as shown, the spindle speed is 280 r.p.m., and feed, 0.004 in. per rev. Of 28-mm. diameter, the hole is 80 mm. long. On the Ceruti machine, the positions of the spindle head and the table can be pre-selected with the aid of stop drums, one of which is seen at the right of the table

Maag (Burton, Griffiths & Co., Ltd.) machines are among those employed in the gear grinding shop for finishing operations on gears for lathes and other machines. Here, a headstock spindle gear for a turret lathe of the 80/100 series is being ground. A roughing and a finishing operation are required, and the total time is 14 hours. Of 236-mm. pitch diameter, the gear has 59 teeth of module 4. The pressure angle is 20 deg., and the face width, 25 mm.



## Camlock Tools with Tungsten Carbide Throw-away Tips

Hillcliff Hard Metals, 54 Woodland Street, Sheffield 6, in association with Marsh Bros. & Co., Ltd., Ponds Steel Works, P.O. Box 82, Sheffield, have introduced a range of lathe tools, fitted with throw-away tungsten carbide tips, which incor-porate a clamping method of outstanding simplicity, that has proved extremely effective in extensive practical tests. These tools are the subject of a patent application, and typical examples from the range are shown in Fig. 1. They are at present being made in shank sizes of % and % in. square, and % in. wide by 1 in. deep, and two designs to take triangular and square tips are available. Square-tip tools can be supplied with approach angles of 5 deg. and 15 deg., and triangular tools with approach angles of zero and 15 deg. The shanks are so designed that one size of square tip, measuring 1/2 in. square by 1/6 in. thick, and one size of triangular tip, of 0.4-in.

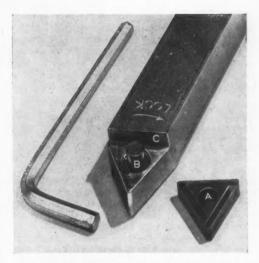


Fig. 2. The Tip is Securely Held in the Holder by the Locking Action of an Eccentric-ended Socket Head Screw

inscribed circle by 78 in. thick, suffice for the entire range of tools.

The method of clamping the tip can be seen in Fig. 2. A centre hole A is provided in the tip, which is engaged by the plain stem, B, of a fain. B.S.F. socket head screw, machined eccentric to the thread by 0.040 in., to provide a cam locking

action. The tip is merely held on the seating by finger pressure, rotation of the screw in the tapped hole of the then securely locks it against the vertical step face. For tightening, the screw must be rotated in a clockwise direction when viewed above, so that it moves downwards, thereby ensuring that the tip is firmly seated on the shank. The shank, it may be noted, is of 0.4 per cent carbon steel. and is case hardened at the seating end to provide resistance against damage from swarf.

Another important



Fig. 1. Camlock Throw-away Tip Tools with Chipbreaker Grooves, Introduced by Hillcliff Hard Metals

feature of these tools is that chipbreaker grooves are formed in each face of the tips, so that the need for separate tool components for this purpose is avoided. The chip-breaker grooves, moreover, provide a positive rake of 8 deg. on the tip, and the shank seating for the latter is formed at a negative angle of 5 deg. Thus, a positive cutting rake of 3 deg. is provided on all the eight edges of a square tip, and on the six edges of a triangular

tip.

The company makes tungsten carbide, and the tips for these Camlock tools are available in five grades. For machining plastics and free-cutting brass, for example, a Grade A tip is recommended, while Grade B is intended for cast iron and nonferrous materials. Grades C and D are titanium tungsten carbides developed, respectively, for rough and finish machining steels. For finish machining steels at high speeds, also for carrying out roughing operations under good conditions, Grade E tips, which also contain titanium, are available. Tips of all grades can be supplied unground, or, if required, ground all over. It is proposed, very shortly, to extend the range of standard sizes, and special shanks to meet customers' requirements can be provided.

Fig. 3 shows a Camlock triangular-tip tool setup for demonstration at the recent Production Exhibition, Olympia, on the stand of Marsh Bros.

Fig. 3. A Camlock Tool Set Up for Demonstration on a Woodhouse & Mitchell 8½-in. Centre Lathe at the 1958 Production Exhibition Held at Olympia

& Co., Ltd., in a Woodhouse & Mitchell 8%-in. centre lathe. With a Grade C tip, a cut %-in. deep was taken on a 3-in. square, black bar of 0.90 per cent carbon steel, at a spindle speed of 480 r.p.m. and a feed of 0.013 in. per rev. On other occasions cuts up to  $\frac{7}{6}$  in. deep were taken at a spindle speed of 682 r.p.m. and a feed rate of 0.017 in. per rev. This Woodhouse & Mitchell lathe is driven by a motor of 10 h.p.

#### **Books Received**

THE ANNUAL REPORT OF THE RURAL INDUSTRIES BUREAU, 1957-58. Rural Industries Bureau, 35 Camp Road, Wimbledon Common, London, S.W.19. 63 pp. [Price 1s. 6d.]

This book gives a comprehensive review of the work of the Bureau during the past year, with details of the instructional visits and courses which were provided. Sections are devoted, for example, to engineering, the experimental workshop, woodworking, and wrought ironwork.

STEEL REVIEW.—THE BRITISH STEEL INDUSTRY. The British Iron and Steel Federation, Steel House, Tothill

Street, London, S.W.1. 64 pp.

This well-designed book provides a comprehensive description of the scope and activities of the British steel industry from all aspects. The text is contained in the centre section, and is flanked by reproductions of a large number of excellent black-and-white and colour photo-

graphs which have been taken at the works of some of the leading steel companies of the country. These illustrations are concerned with the major steel producing and working processes, also the applications of the finished product in its various forms. Copies of the publication can be obtained, free of charge, from the Federation at the above address.

Non-destructive Methods for the Examination of Welds. British Welding Research Association, 29 Park Crescent, London, W.1. 78 pp. [Price 7s. 6d.]

The last of a trilogy which forms the B.W.R.A.'s handbook on non-destructive testing, this booklet (T. 29/1) replaces an earlier publication, No. T.29, which was first issued in March, 1952. Fully-illustrated with photographs and line drawings, it incorporates the results of recent research, and chapters are devoted to the radiographic, ultrasonic (and other acoustical), magnetic, penetrant, and gas leak testing methods, also the proof or overload test and semi-destructive methods. There is a glossary of terms used in radiography, and two appendices concerned with the defects in welds revealed by various methods of examination, and application of these methods to the different forms of welded

## News of the Industry

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Ex-Cell-O Corporation (Machine Tools), LTD., are busily employed on home and export orders for both standard and special, precision fine boring machines. In a walk through the works, we noted a number of standard Junior and Senior types, both single- and double-ended, for a variety of operations. Special machines for the motor car industry include transfer types for machining differential carriers, and for 4-cylinder blocks, two at a time. Two 3-way machines, with inclined slides, are designed for subsequent machining operations on differential carriers received from the transfer machine, while two other 3-way machines, with inclined slides, are for boring and facing operations on the axle housings and banjo casings of rear axle assemblies. We also noted four machines for cutting bearing bores and spherical seats in differential cases, and four machines, two for semi-finishing and two for finishing, connecting rod bores.

Other interesting machines, to which our attention was drawn, are for fine boring brake drums, hubs and oil pump bodies, also for fine turning differential cases, turning and boring cylinder liners, and fine boring conveyor chain links, the latter machines having automatic hopper feeds. Two special 6-spindle machines under construction are for boring suspension arms, and two other large machines on order are for radial grinding operations on the roots of gas turbine blades. We also noted a 2-head machine for boring, facing and chamfering operations on starter ring gears. Two machines for operations on commercial vehicle axle arms and another for crankcases are being built for export to France. At a later date, it is hoped to make further reference to some of these interesting machines.

SPENCER GEARS, LTD., are steadily occupied on a variety of gear-cutting work, which includes spur, helical, straight and spiral bevel, and worm gears, also racks. Other services provided are gear grinding, flame-hardening of gear tooth profiles, industrial paint-spraying, stove-enamelling, shotblasting and metal-spraying.

PERCY MARTIN, LTD., have an extensive and varied range of new and reconditioned machine tools available for immediate delivery from their Melton Road and De Montfort Street works.

J. W. BAMKIN & Co. are engaged on the pro-

duction of air-operated, automatic, universal single- and double-ended stud threading machines, cam-operated single- and double-ended stud threading machines, and tool and cutter grinding machines. Special machinery orders and subcontract component assembly work are also in hand.

Burrows & Smith, Ltd., have a good programme of sub-contract orders in progress, comprising a large batch of Fellows gear shaping machines, which they are building for Alfred Herbert, Ltd., Coventry, and a variety of components for the diesel oil engine industry. Automatic loading equipment is being provided on some of the gear shaping machines.

WYVERN MACHINES, LTD., are doing a steady

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Recently supplied by Dale Electric (Yorkshire), Ltd., Filey, Yorks., to the British Transport Commission, this mobile battery charging unit has a rating of 24/32 volts, 62/47 amp. The 1·5-kW. shunt-wound generator is driven at a speed of 2,600 r.p.m. by a Villers 4-stroke, air-cooled engine, and output is indicated by a voltmeter and ammeter on the control panel. There is also a field voltage regulator, automatic battery cut-out switch, and a main switch. Weather protection is provided by a removable cover

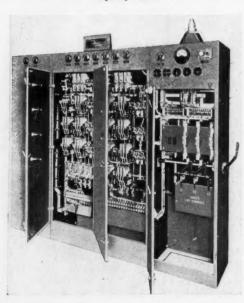


trade in 7½ and 8½ in. centre and capstan-type lathes, some of which are equipped with hardened steel bed slideways and hydraulic copying mechanism. On export account, we may note orders for Canada and South Africa. The associated TOMBLIN MACHINERY, LTD., have a variety of machine tool reconditioning work in progress.

RUDKIN & RILEY, LTD., report a good home and export demand for die shop machinery, comprising piercing and polishing equipment for the treatment of wire, rod and tube drawing dies. Export markets include Australia, New Zealand, South Africa and India. In addition, we may note orders in hand for the GKN spark erosion machine, electromagnetic crack detectors, and precision internal and external cylindrical grinding machines. We hope shortly to describe a recently-developed coil spring end grinding machine and an internal

. . .

The illustration shows a contactor-type switchboard fitted with magnetic overload releases, and signalling arrangements by means of coloured lamps, made by Erskine, Heap & Co. Ltd., Manchester, to the order of the Fairey Aviation Co. Ltd., for use on the Fairey-Ferranti tape-controlled milling machine described in MACHINERY, 92/932—25/4/58. This switchboard controls the power for the motor drive and sequences of operation initiated by the electronic system of the machine, and it incorporates 15 contactors of various sizes, 10 relays with associated interconnections, and a 400-amp isolating switch with high rupturing capacity fuses.



grinder equipped with radius grinding attachment.

DECO MACHINERY, LTD., are doing a good home and export business in fine strip rolls, also spooling and drawing machinery. Our attention was drawn to an interesting attachment which has been developed for straightening wire prior to rolling or drawing. To facilitate the insertion of the wire between the upper and lower rolls, a single-lever, cam-operated mechanism ensures rapid opening and closing of the rolls, and it is hoped to make further reference to this in due course. Extensions now in progress at these works will add 3,500 sq. ft. to the floor space of the erecting shop. Recent additions to plant include two Ward No. 7 capstan lathes, an Archdale 4 ft. radial drilling machine, and a Jones-Shipman 40- by 10-in. cylindrical grinding machine.

HARBOTS, LTD., are experiencing a brisk demand for their precision hydraulic surface grinding machine, and orders are in hand from Canada. Australia, India and South Africa. It is hoped shortly to have available a surface grinder, equipped with a 10- by 18-in. table, to meet the particular needs of die and mould makers. A steady business is reported in slip gauges and machinists' gauge blocks, and other work in hand includes precision flat and circular form tools, profile-ground press tools, special milling cutters, comparators and gauges. An Archdale milling machine and Colchester and Harrison lathes have recently been added to the plant.

LEICESTER MACHINE TOOL Co. were occupied, at the time of our call, on a variety of machine tool reconditioning work, which included a Herbert No. 4 Senior lathe, a Ward combination turret lathe and a Kearns horizontal boring machine.

THE JAY-EFF FLAME HARDENING Co. are finding a well sustained demand for a variety of flame-hardening work by the Shorter process, and components are being treated in carbon and alloy steels, plain and alloy cast irons, Meehanite and malleable irons. Among the work recently treated we may note gears, cams, shafts, drums, rolls, levers, dogs, clutches, machine beds, slides and spindles.

H. C. PRETTY & SONS, LTD., report a satisfactory call for power transmission equipment, including belting, cast-iron pulleys and V-rope drives, and the repetition machining department is busily employed. The associated H. C. PRODUCTS, LTD., are finding a steadily widening application, particularly in the motor car industry, for the Taskmaster planning and progress system.

DALLOW, LAMBERT & Co., LTD., Thurmaston,

are well employed on the production of small, medium and large-capacity dust collecting units, which include standard Drytex, Dustmaster and wet Deduster types. Some of the firm's equipment is on view on the stand of the Birmingham Engineering Centre Group at the Brussels World Exhibition.

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NICOR DESIGNS, LTD., Worcester Street, Wolverhampton, are busy with the design and planning of special-purpose units and complete transfer machines, several of which are destined for the aircraft industry. The premises, in which modern drawing office equipment is installed, are well appointed. At present more than 40 draughtsmen are employed on work which ranges from the design of a small component, to the detailing of the complete tooling for a new engineering product. When circumstances permit, arrangements can be made for special-purpose equipment, designed here, to be constructed in the shops of an associated company.

ROBERT HARRIS, LTD., Waddens Brook, Wednesfield, Staffordshire, are busy with the production of pressings for a range of exhaust silencers, fuel tanks and other accessories for internal combustion engine units. Several large presses are

installed, including 150and 200-ton machines by Wilkins & Mitchell, the former having been delivered recently. Delapena radio frequency induction heating equipment is employed for brazing fittings to small petrol tanks, the cycle time for this operation being 10 sec. Exhaust silencer pressings are assembled by seam by welding. Other facilities at these works include a Parkerizing plant and a tool room.

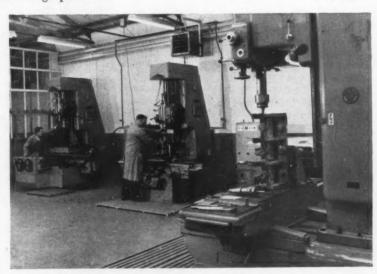
VILLIERS (TOOL DEVELOPMENTS), LTD., Waddens Brook, Wednesfield, Staffordshire, a subsidiary of The Villiers Engineering Co., Ltd., Wolverhampton, have modern works with

an area of 18,000 sq. ft., and it is planned to provide extensions, in the near future which will increase the space to 30,000 sq. ft.

This newly-established company is engaged in design and production of jigs, tools and special purpose machines for the parent firm, and to a greater extent for the engineering trade generally. Part of the works is laid out specially for the construction, and testing under working conditions, of transfer and other special purpose machines, and large fixtures. The machine shop is equipped with modern machine tools, most of which were new when they were installed. They include a 36-in. open-side and a 10- by 5- by 5-ft. planing machine; centre, turret and capstan lathes; machines for die sinking; and a range of grinding machines and boring equipment. The jig boring enclosure is large enough to house six machines, but so far only three have been provided-two by Newall and one by Kolb, as shown in the illustration. On the left is seen a Newall 2436 optical jig borer, stated to have been the first of its type to be supplied to a user.

The Kolb machine is shown with a fixture more than 30 in. high mounted on the table. There is a standards room, provided with modern inspection equipment, and a drawing office, with accommodation for ten draughtsmen, has recently been brought into operation.

F. W. H.



Part of The Jig Boring Enclosure at the Works of Villiers (Tool Developments), Ltd. Three Additional Jig Boring Machines are to be Installed in this Department

#### Nottingham

MYFORD ENGINEERING Co., LTD., Beeston, have a good volume of home and export orders in hand for their M.L.7 and Super 7 lathes, of 3½ in. centres, M.L.8 woodturning lathes, and M.G.12 cylindrical grinding machines. Recent innovations include a swivelling workhead for the cylindrical grinding machine, to which we hope to refer again, and a mortising attachment for the woodturning lathe. Lathes have recently been supplied for testing and truing brake drums. The latest addition to plant is Delapena honing equipment.

RAGLAN ENGINEERING Co. (1954), LTD., have lately noted some expansion in the home and export demand for the Little John 5-in. centre and capstan lathes. These machines have recently been exported to Nigeria, Ghana, Hong Kong, Sudan and the U.S.A., for example.

THE VALUE OF EXPORTS from this country of all types of machinery (other than electric) during the first six months of this year was £289,663,488. The corresponding figure for 1957 was £282,997,691, and for 1956, £260,207,707.

#### Developments in Tool Servicing Arrangements

(Continued from page 287)

Once it has been ensured that tools will be replaced regularly, it remains to provide for rapid interchange. Clearly, if delay is to be avoided, duplicate, sharpened tools must be available, and it is usual to make provision for the storage of such tools in conjunction with the tool-life indicating dials, where they are installed. It is equally necessary to employ tool holders which permit of presetting with the aid of simple fixtures and gauges. Actual replacement of tools on a machine is then a rapid and virtually unskilled operation. As an indication of the results than can be obtained in this manner, it is reported that nine tools employed in an experimental set-up on a multi-spindle automatic, for machining a sparking plug body, can be changed in 5 min. 40 sec. Without pre-set, quick-change holders, the time required was 42 min. 35 sec. This particular machine operates on a 4½ sec. cycle, and the time saved during one tool change represents an output of 492 parts.

The principle to be observed, clearly, is that the more expensive and productive the machine installation, the more important is correct tool selection and/or sharpening, and regular and rapid

changing.

#### Machine Tool Exports and Imports

	Month ended		ths ended
Type of Machine	April 30, 1958	1957	1958
	Value £	Value £	Value £
New, complete-			
Boring machines: Vertical	10.315	110,899	110.43
Other	19,315 75,248	299,458	274 457
Drilling machines	91,675	774,155	646,078
Grinding (excluding thread	71,073	777,133	010,071
grinding), lapping and			
honing machines	200,585	855,329	742.570
Lathes:			
Automatic	97,169	663,048	505,893
Capstan	208,217	961,160	733,000
Other	248,393	1,039,617	967,99
Screwing machines Threading machines	9,320	818,08	67,70
Threading machines	11,336	247,581	137,350
Milling machines (excluding			
thread-milling and gear cutting machines)	125 242	777.044	904 97
Planing, shaping and slot-	125,342	777,064	804,87
ting machines	61,061	249,598	310,95
Presses:	01,001	217,370	310,73.
Hydraulic	26,670	417.249	214.26
Other	66,325	293,357	420.29
Punching and shearing			
machines	45,308	149,651	154,686
Other plate and sheet			
metal-working machines			
including straightening rolls	00 222	92 449	172 00
All other machines	88,232 206,833	92,449	936,86
Used machines, complete	77,095	231,877	243,070
Parts	172,806	756,460	759,65
Total	1,830,930	9,054,723	8,202,14
Destination		2.5.0.	
Union of South Africa	144,145	469,693	644,47
ndia	208,343	1,240,677	1,227,09
Australia	279,481	1,317,164	1,222,88
New Zealand	28,321 150,965	138,370 566,070	147,48 631,84
Other Commonwealth coun-	130,763	300,070	631,04
tries	110,213	565,837	597,36
Soviet Union	20,528	426,785	63,74
Sweden	62,979	336,871	195,25
Western Germany	47,692	214,270	161,82
Netherlands	48,562	313,515	175,65
France	124,126	733,046	676,23
Spain	93,555	401,940	431,96
taly	67,611	231,175	344,78
U.S. America	137,219	932,052	458,16
Other foreign countries	307,190	1,167,258	1,223,36

New, complete—		1	1
Boring machines	49,405	955,775	364,028
Drilling machines	20,150	105,583	91.291
Gear-cutting machines Grinding, lapping and	102,397	426,629	196,912
honing machines	186,175	867,229	863,195
Automatic	243,859	730.854	1,015,725
Other	15,338	110,153	106,479
Milling machines	163,251	761,618	773,962
ting machines	4,601	154,616	74,109
Presses	79,897	248,520	278,072
All other machines	470.295	1.454.768	1,461,421
Used machines, complete	144.816	84,204	236,410
Parts	282,019	1,558,399	1,175,713
Total	1,762,203	7,458,348	6,637,317
Country of Origin			
Western Germany	620,287	3,140,023	2.334,928
Switzerland	225,060	827,478	1.060,353
U.S. America	610,571	2,428,941	1,788,248
Other foreign countries	306,285	1,061,906	1,453,788

#### Letters to the Editor

[The Editor does not hold himself responsible for the views expressed by his correspondents.]

#### Practical Examples of the Applications of Ceroc Sintered Ceramic Cutting Tools

(To the Editor of MACHINERY)

SIR,—Having read the article under the above heading in Machinery, 93/20—2/7/58, I respectfully suggest that it could have carried a sub-title "Practical Examples of the Mis-application of Tungsten Carbide Cutting Tools."

It is the publication of this type of information, based on entirely false comparisons, which is tending to mislead industry concerning the relative merits of sintered oxide and sintered carbide tooling. In no case has the grade of carbide been mentioned or any details of tool geometry furnished. It is quite obvious to the experienced eye, from the data quoted, that incorrect grades of carbides were in use, particularly with reference to the vertical boring of workpiece B and the planing operation.

A comparison of the good utilization of oxide tips with poor utilization of carbide serves no purpose whatsoever, indeed it would be simple to write an article to produce the reverse picture based on similar "evidence." The purpose of this letter is not to deprecate the performance of the particular sintered oxide tool used, except to say that we would certainly expect to employ Wimet sintered carbides successfully at the speeds mentioned for that oxide material.

Furthermore, reference to steels merely by their tonnage is of little value when considering relative machinability of British, American and Continental steels. Such comparisons may only usefully be made from full analyses of the steels, the heat treatment conditions being known, and reference to photomicrographs of the structures.

Wickman, Ltd., R. N. Соок, arch and Development Manager,

Research and Development Manager,
Coventry. Wimet Division.

#### **Trade Publications**

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CHEMICAL PIPE & VESSEL Co., LTD., Godstone Road, Kenley, Surrey. Catalogue giving full dimensional particulars of the company's range of polythene tubes and fittings for plumbing. The advantages of this material for such purposes are described, and information is included on the procedure for welding polythene, also its chemical and physical properties.

ROTAX, LTD., Willesden Junction, London, N.W.10. Brochure describing typical applications of magnetic amplifiers to aircraft electrical systems, and indicating the extent of their use and the advantages which are claimed for this type of equipment. The publication includes photographs and theoretical diagrams, also a layout drawing for a typical aircraft generating system.

Taylor Woodrow (Building Exports), Ltd., 41 Welbeck Street, London, W.1 (a member of the Arcon Group). Well-illustrated brochure showing some of the more recent applications of the Arcon sawtooth-roof building, both in this country and overseas. Advantages claimed include speed of erection; clean shape, both internally and externally; maximum utilization of natural light; and the fact that it may readily be extended.

FRY'S METAL FOUNDRIES, LTD., Tandem Works, Merton Abbey, London, S.W.19. Booklet with loose pages, in a stiff card cover, entitled "The Flowsolder Method of Soldering Printed Circuits." A feature of the Flowsolder machine (see Machinery, 89/1469—28/12/56) is that heated solder is continuously circulated through an 8-in. wide nozzle in the bath so that it is delivered in a wave form. Printed circuits up to 7½ in. wide, and of virtually any length, are moved in a straight path in contact with the crest of the solder wave. The booklet comprises different sections which give details of and working instructions for the Flowsolder machine, particulars of Flowsolder alloys, and information concerning the actual soldering process.

#### Coventry Gauge Rockwell Merger

The directors of Coventry Gauge & Tool Co., Ltd., and of Rockwell Engineers, Ltd., announce that they have realled agreement, in principle, as to a merger of the two concerns. It is envisaged that this will be achieved by the acquisition by Coventry Gauge & Tool Co., Ltd., of the whole share capital of Rockwell Engineers, Ltd. Accordingly, and subject to agreement in detail and to C.I.C. consent, it is the intention of Coventry Gauge & Tool Co., Ltd., soon to make a formal offer to acquire the whole share capital of Rockwell Engineers, Ltd., in consideration of the issue of 5 Coventry Gauge & Tool Co., Ltd., ordinary stock units of 10s. each for each 4 Rockwell Engineers, Ltd., ordinary shares of 5s. each.

Mr. C. E. Rockwell and Mr. John Middleton would, on completion, join the board of Coventry Gauge & Tool

The Rockwell Machine Tool Co., Ltd., would continue to operate under the same name.

#### Correction

In the advertisement for Panton & Webb, Lavender Hill, Tonbridge, Kent, which appeared on p. 103 of Machinery for July 30, the description accompanying the first illustration should have read: "The latest addition to a range of all-British fine-pole permanent magnetic chucks. The working area is 14 in. by 12 in." The correct designation of the second item is: "The Fimax 73 S.B. universal magnetic chuck."

#### **Industrial Notes**

INCORPORATED PLANT Engineers announce that their head office is now at 2 Grosvenor Gardens, London, S.W.1 (telephone number, Sloane 0469).

THE PALNUT Co., LTD., inform us that they are now occupying their new works and offices. The address is Palnut Works, 3 Arthur Street, Hove, 3 (telephone number, Hove 70427).

BABCOCK & WILCOX, LTD., 209 Euston Road, London, N.W.1, inform us that their collaboration with the American company of the same name is to be extended to include technical co-operation in the field of nuclear power.

AN AUCTION SALE OF MACHINE TOOLS and miscellaneous stores from Technical Stores Depot, Old Dalby, Melton Mowbray, will be held on September 3. The auctioneers will be Shouler & Son (Dept. N), 1 Norman Street, Melton Mowbray.

PERMALI, LTD., Bristol Road, Gloucester, have recently installed a polytetrafluorethylene sintering oven with internal dimensions of 6 by 6 by 15 ft. long. This oven enables the dispersion coating process to be applied to such large items as tanks, rollers, and containers, for example, and is also being used for sintering solid P.T.F.E.

THE ALUMINIUM DEVELOPMENT ASSOCIATION, 33 Grosvenor Street, London, W.1, have issued the 1958 editions of the following publications: Directory of Members; List of Publications; and List of Films, Film Strips, and Wall Charts. These publications are available, on request, from the above address.

The British Iron and Steel Federation, Steel House Tothill Street, London, S.W.1, has issued a booklet entitled "The Steel Industry's Labour Record." Sections are included under the sub-headings: comparison with other industries; negotiating machinery; and unions in the industry.

APPLEBY-FRODINGHAM STEEL COMPANY, a branch of the United Steel Companies, Ltd., inform us that the new steel plate rolling mill at their Scunthorpe works is now in operation. This 12-ft., 4-high mill is powered by twin 4,000-h.p. D.C. motors, and the minimum thickness of plate that can be rolled is  $\frac{1}{4}$  in. For plates  $\frac{1}{2}$  in. thick, the maximum width is 11 ft. 6 in.

The 1959 Nuclear Congress will be held at Cleveland, Ohio, U.S.A., from April 5 to 9, and more than 150 papers will be presented on such subjects as reactor design, disposal of radioactive wastes, radiation shielding, and instrumentation. Particulars can be obtained from the Engineers Joint Council, 29 West 39th Street, New York 18, New York.

ADA (HALIFAX), LTD., Pellon Lane, Halifax, producers of washing machines and spin driers, have recently acquired Mile Cross Sheds, Halifax, with a floor space of 30,000 sq. fu., which were formerly occupied by Courtaulds, Ltd. It is proposed to develop a fully-automatic factory which, eventually, will be capable of producing 2,000 refrigerators per week. This project, estimated to cost £150,000, will

include the provision of a fully automatic stove-enamelling plant, electro-static paint spraying equipment, and other new machinery.

THE BIRMINGHAM COLLEGE OF TECHNOLOGY has organized a series of one-day conferences on electronic digital computers and their industrial applications. The first of these conferences, which will have special reference to Ferranti computers, is to be held on October 8, and full details of the complete series can be obtained from the Registrar, College of Technology, Gosta Green, Birmingham, 4.

STEEL CENTENARY.—A ceremony was held recently to commemorate the 100th anniversary of the first mass production of ingot steel in the world, on the original site of the old blast furnace at Edsken in Sweden. This furnace was erected by G. F. Göransson in 1857 for experiments with the production of steel according to the Henry Bessemer process. In July, 1858, Göransson finally succeeded in producing steel by this method.

MOTOR CAR PRODUCTION.—British motor-car production in the first six months of the year reached a new high level at 550,699, compared with 388,572 in the same period of last year. Motor car exports also reached a new peak at 250,883, during the first half of the year, compared with 204,946 in the corresponding period last year. In the first quarter, car exports totalled 132,323, and in the second quarter, 118,560.

AIRMEC, LTD., High Wycombe, Bucks., recently entered into an agency agreement with Apparacchi Scientifici Federici, of Milan, whereby they hold the exclusive rights to market in the United Kingdom ultrasonic drilling and ultrasonic medical equipment made by the latter organization. The ultrasonic drilling equipment permits of cutting intricate forms in ceramics, hard metals and other materials.

J. Broughton & Son (Engineers), Ltd., 234 Pershore Road South, Birmingham, 30, inform us that the manufacture and marketing of their range of mechanical guards for presses, milling machines, die casting machines, and similar equipment, has been transferred to a subsiduary company, Piant Inspection & Control, Ltd. These products will still be known as Broughton guards and the manufacture and marketing of all other equipment will be continued by the parent company.

THE WICKMAN FILM UNIT has recently made the first of a quarterly magazine series entitled Facts and Faces. In black and white, with sound, it is concerned with various new Wickman products and developments, and runs for 14 min. Other Wickman films include Wimet at Work, Designing and Applying Carbide Tools, The Wickman Erodomatic and Impact Extrusion. All, including the first, Facts and Faces, are available on loan from the Publicity Department, Wickman, Ltd., P.O. Box 44, Coventry.

G. & J. Weir, Ltd., Cathcart, Glasgow, S.4, and Catton & Co., Ltd., 29 Chadwick Street, Black Bull Street, Leeds, 10, are to combine their foundry activities,

and for this purpose a new company known as Weir-Catton, Ltd., is being formed. This company will acquire the capital of Catton & Co., Ltd., also that of the Argus Foundry, Ltd., which is at present a wholly-owned subsidiary of G. & J. Weir, Ltd. Under the new arrangement, the name of Argus Foundry, Ltd., will be changed to Weir Foundries, Ltd.

BOROUGH POLYTECHNIC, Borough Road, London, S.E.1, are holding an evening course in work study, which will start on September 22. This course is intended primarily for students who have already qualified for parts I and II of the Production Engineers Examination, and who desire to prepare for the work study examination in part III under the existing regulations for 1958-9. A syllabus may be obtained on application to the Department of Mechanical Engineering, at the above address.

S. Parsons & Co., Ltd., St. George's Ironworks, Young, Street, Bradford, have developed special equipment for weighing and checking the centre of gravity of, the new Armstrong-Whitworth AW 650 Freightercoach aircraft. There are separate weighbridges for the two main wheels, and a nose wheel weigher, which is mounted on a mobile lift constructed by Shorts Lifts, Ltd., Bradford. It is stated that preliminary tests have indicated that the equipment will operate with a total error of 4 lb. for loads up to 60,000 lb.

PLANNAIR, LTD., Epsom Road, Leatherhead, Surrey, are building a new factory at Leatherhead which will add 15,000 sq. ft. of floor area to their existing capacity. This new factory, which is scheduled for completion in October, will incorporate research laboratories equipped with high and low temperature cabinets capable of simulating all climatic conditions. Plans are also in hand for a further extension, of 4,000 sq. ft., which will provide additional factory space and administrative offices. When these buildings are completed and in full production, it is stated, the company's output will be trebled.

ROBALLO ENGINEERING Co., Ltd., 43 Dover Street, London, W.1, a newly-formed English company, have been granted exclusive marketing rights in Great Britain for Roballo ball bearing slewing rings and it is stated that arrangements have been made for their production in this country. The slewing rings, to which reference has previously been made in Machinery, 91/1435—20/12/57, are intended for application to slewing cranes, excavators, derricks, revolving fire ladders, turntables and similar equipment. In addition, the company will supply large-diameter wire-race ball bearings for continuously rotating machinery.

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The American Society for Testing Materials has published volume 57 of the Proceedings, covering the year 1957. This publication, which extends to 1,430 pp., covers the technical activities of the Society during that year, and includes reports and papers presented during the year and accepted for publication, also discussions. A summary of the proceedings of the A.S.T.M. 60th annual meeting, and the Philadelphia Spring Meeting is given, together with a programme for each session, indexed by title and author. Copies of the publication can be obtained

from the A.S.T.M., 1916 Race Street, Philadelphia 5, Pa., U.S.A., price \$12.

WINSTON ELECTRONICS, LTD., Shepperton Middlesex, announce that they have organized extensive installation and maintenance facilities for the range of electronic equipment which they are marketing for Beckman Berkeley and Berkeley Helipot, Calif., U.S.A. The range includes electronic and magnetic counting, reading, and timing instruments, time interval meters, frequency measuring apparatus, digital recorders, pulse generators, scintillation counters, oscillators, and Helipot precision potentiometers. The latter are available in 16 basic designs, and are now being produced by Beckman Instruments, Ltd., the new British subsidiary of Beckman Instruments, Inc., U.S.A. at their factory at Glenrothes, Fife, Scotland.

City and Guilds of London Institute, Gresham College, Basinghall Street, London, E.C.2, announce a new course on engineering drawing which will start in the next session. The course includes applied mathematics, mathematics and geometry, and materials and processes, and is intended for students who have attained the S.3 level in the National Certificate (Mechanical) course, or hold an intermediate certificate in machine shop engineering, or the appropriate final certificate. Provision is also made for older students who have already gained drawing office experience. Enquiries concerning this new course should be marked "B.5," and sent to the Director of the Institute at the above address.

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#### Alfa-Laval Anniversary

A well-presented and illustrated brochure has been issued in connection with the 75th anniversary of the formation of the Alfa-Laval/De Laval Group of Companies. The parent firm-the Separator Company, Stockholmwas formed in 1883 to exploit Dr. Gustav De Laval's invention of the first continually operating cream separator.

Products of the Group now include cream separators and other farm and factory dairy equipment, centrifugal separators for oil and other liquids, heat exchangers, stainless steel pumps, textile machinery, car body pressings, washing machines, and agricultural machinery.

The British organization (Alfa-Laval Co., Ltd.), with factories at Brentford, Middlesex, and Cwmbran, Monmouthshire, has a substantial production of milking machines, centrifugal separators, filters, pumps and heat exchangers.

#### Cold-pressure Welding

In Machinery, 93/207-23/7/58, was published an article entitled some applications of cold-pressure welding. We are asked to point out that the process there described was developed by the General Electric Research Laboratories, East Lane, North Wembley, Middlesex (see Machinery 73/832-16/12/48), to whom all enquiries concerning applications in this country should be addressed.

#### Personal

Mr. R. J. Barritt has been appointed chief executive, Engineering Division, The British Oxygen Co., Ltd., Bridgewater House, Cleveland Row, St. James's, London, S.W.1. He will take up his duties on September 1.

MR. FRED COOPER has retired, at the age of 71, after 59 years' continuous service with Geo. Salter & Co., Ltd., West Bromwich, Staffs. His brother, Mr. Frank Cooper, who is aged 73, is still employed with the company, which he joined 60 years ago.

MR. J. BETTS, who was formerly with Taylor, Taylor & Hobson, Ltd., has joined the staff of Gamet Products, Ltd., Hythe, Colchester, as technical sales engineer. He will cover the Midland area and starting in September will operate from, 54 Hidcote Road, Oadby, Nr. Leicester.

MR. J. N. HEMSLEY is retiring after representing Deloro Stellite, Ltd., Highlands Road, Shirley, Birmingham, in London and Southern England, for more than 20 years. As a sales engineer and specialist in Stellite hard-facing and cutting tools, he is widely know in the area.

Mr. Edward E. Toon has been appointed managing director of Stern & Bell, Ltd., Stour Street; Birmingham, with whom he has held the position of works director since 1950. He recently succeeded Sir Graham Cunningham as managing director of Weldall & Assembly, Ltd., Stourbridge, Worcs., and is also chairman of Charles S. W. Grigg, Ltd., Hounslow, all the companies mentioned being members of the Triplex Engineering Group.

MR. SIDNEY ALLEN, M.I.Mech.E., F.R.Ae.S., has been appointed chief engineer for all products of Armstrong Siddeley Motors, Ltd., Parkside, Coventry, except motor cars. He was formerly chief engineer (rockets).

In addition to their aero engines, motor cars and rocket engines, the company are now building air-cooled diesel engines, auxiliary gas turbines and air starters, and will build the large Maybach diesel engines under licence.

#### Scrap Metals

LONDON.-Prices per ton for non-ferrous scrap metals free from iron are as follows:-clean copper wire, untinned and free from lead and solder, £160; clean heavy copper, untinned and free from lead and solder, £154; second grade copper wire, £147; clean light copper, £142; braziery copper, £126; gunmetal, £129; brass mixed, £92; lead, net, £56; zinc, £29; cast aluminium, £84; old rolled aluminium £107; battery lead, £29; unsweated brass radiators, £78; hollow pewter, £495; black pewter, £365.

MIDLANDS.—Trading, which has been carried on at reduced tempo over the past few months, has practically come to a standstill with the advent of the annual industrial two weeks' holiday. Steelworks and foundries are not accepting deliveries and blast furnaces are taking limited tonnages only.

Yards are fully stocked with all grades of scrap, a large proportion of which consists of processed material for which no markets are open. Discussions in connection with the export of scrap are reported, and merchants will hope that the position may thus be eased in the difficult weeks ahead.

Prices are still falling, due to the fact that many tons of production scrap will have to be stored indefinitely until such time as consumers can accept deliveries without restriction. Even heavy scrap is difficult to place and local steelworks will not be giving out allocations until the end of August.

Light scrap is still being "tipped" in many areas as there is little demand for either No. 5 material or hydraulically compressed destructor bundles.

Although the Control Order covering maximum selling prices is still in forme the prices of many grades are now far below the maximum and merchants have reduced their offers accordingly.

Light scrap is not wanted, apart from limited quantities of light steel cuttings for pressing, and bushy turnings are practically unsaleable.

No improvement is expected until towards the end of the year.

Current maximum control prices, delivered consumers' works, are now: \*Heavy steel No. 1, 217s. 6d.; \*heavy steel No. 2, 196s.; \*heavy steel No. 4, 207s. 6d.; \*heavy steel No. 5, 195s. 6d.; light iron No. 8, 149s.; short turnings No. 9 (free from alloy), 167s. 3d.; light steel No. 11, 164s. 3d.; bushy turnings, 117s.; short alloy turnings, 160s. 9d.; short steel No. 2, 233s. 3d.; machinery cast,

Prices may be increased up to 2s. 6d. per ton according to quantities tendered over a given period.

<sup>\*</sup> For use by Round Oak Steelworks, Brierley Hill, increase by 18. 6d. per ton.

† George Cohen, Sons & Co., Ltd., 600 Commercial Road, E.14.

‡ Subject to market fluctuations.

#### International Institute of Welding

The tenth Annual Assembly of the International Institute of Welding, recently held in Vienna, was attended by some 800 delegates from 27 countries, including Great Britain, and France. It may be noted that the U.S.S.R., Yugoslavia, and the Argentine were represented for the first time. As a result of the meeting, some 30 documents are to be issued for publication, among which the following may be noted: results of an international investigation on residual stresses and stress relieving; effect of localized heat treatment on the fatigue behaviour of welded joints; particular instances of cracking caused by fatigue; training and quali-

fication of engineers, technicians, and welders; welding problems in parts of the Atomium of the Brussels Exhibition; and recommendations for the classification of steels for welded constructions.

The work of the International Institute of Welding is carried on by 15 technical commissions and includes the publication of literature such as the quarterly, Bibliographical Bulletin for Welding and Allied Processes, a multilingual collection of terms for welding and allied processes, and a collection of reference radiographs of welds.

The affairs of the Institute are administered in this country by the Institute of Welding, 54 Princes Gate, Exhibition Road, London, S.W.7.

#### Machine Tool Share Market

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of

The general undertone of stock markets was firm during the period under review, but mainly quiet conditions prevailed in most sections, with buying interest selective, and price changes were generally small and irregular.

The gilt-edged section sustained a moderate turnover, but after it had remained steady to firm for the most part, an easier tendency developed, and quotations of British Funds, also home corporation and Dominion stocks, finished with slight declines on balance.

In the principal sections of the industrial share market a satisfactory undertone was maintained. Although activity never reached a high level, and movements among prices generally were moderate, the trend, for the most part, was towards higher levels, and a few good features developed.

Among machine tool issues, Birmingham Small Arms advanced 3d. to 27s. 9d.; British Oxygen, 1s. 3d. to 37s. 9d.; Broom & Wade, 4½d. to 11s. 3d.; Chas. Churchill, 1½d. to 4s. 10½d.; Geo. Cohen, 6d. to 11s. 3d.; and John Shaw & Sons (Wolverhampton), 1½d. to 11s. 7½d. On the other hand, Coventry Machine Tool lost 6d. at 8s. 3d.; and John Harper, 3d. at 12s. 6d.

COMPANY		Denom.	Middle Price	COMPANY		Denem.	Middle Price
Abweed Machine Toels, Ltd			9d.	Harper (John) & Co., Ltd	Ord	5/-	12/6xd
Armstrong, Stevens & Son, Ltd Allen (Edgar) & Co., Ltd	Ord	()	8/3		41% Red. Cum Prf.	£ì	13/14
	5% Prf	13	14/9*	Herbert (Alfred), Ltd	Ord	£I	35 /
Arnott & Harrison, Ltd		5/-	18/9	Holroyd (John) & Co., Ltd	"A" Ord	5/-	10/6
	6% Cum. Prf.	13	18/6	Jones (A. A.) & Shipman, Ltd	Ord.	5/-	10/3
Birmingham Small Arms Co., Ltd	Ord	£I	27/9		7% Cum. Prf.	5/-	5/-
23 25 444	5% Cum.	13	15/6	Kayser, Ellison & Co., Ltd	Ord	61	18/3
	6% Cum	13	17/6	Kendall & Gent, Ltd.	Ord.	5/-	7/74
01 00 00	6% Cum B" Prf.	-		Kerry's (Gt. Britain), Ltd	Ord		6/3
D 00 00 00 000		Sek.	26 !	Kitchen & Wade, Ltd	Ord		11/6
	Deb.			Martin Bros. (Machinery), Ltd	Ord		2/44
British Oxygen Co., Ltd	Ord	£1	37/9	Massey, B. & S., Ltd.	Ord		8/3
Brooke Tool Manufacturing Co., Ltd.	61% Cum. Prf.	5/-	4/9	Modern Engineering Machine Tools	Ord	3/-	10/74
Broom & Wade, Ltd		5/-	11/3	Newall Engineering Co., Ltd	Ord	2/-	4/6
	6% Cum. Prf.	(1)	17/9	Newman Industries, Ltd	Ord		2/3
Brown (David) Corporation Ltd	54% Cum. Prf.	£I	14/-		6% Prf. Ord.	5/-	5/6x
Buck & Hickman, Ltd	6% Cum. Prf.	13	17/9	Noble & Lund, Ltd.	Ord		2/9
Butler Machine Tool Co., Ltd	Ord	5/-	6/3	Osborn (Samuel) & Co., Ltd	Ord		18/-
C.V.A. Jigs, Meulds & Tools, Ltd	5% Cum. Prf.	£1	13/9	D(E) 9 C- 1-1"	51% Cum. Prf.	£1 5/-	26/-
C.V.A. Jigs, Meulds & Tools, Ltd	54% Red.	2.1	13/7	Pratt (F.) & Co., Ltd	Ord.		5/-
Churchill (Charles) & Co., Ltd	Ord	2/-	4/104	Ltd.	W144	1	31
	6% Cum. Prf.	13	26/3	Shardlow (Ambrose) & Co., Ltd	Ord	EI	36/9
Churchill Machine Tool Co., Ltd		S/-	17:71				
C. P. C	6% Cum. Prf. Ord.	5/-	18/6	Shaw (John) & Sons, Wolverhamp- ton, Ltd.	Ord	5/-	11/74
Clarkson (Engrs.), Ltd	Ord		11/3	Sheffield Twist Drill & Steel Co., Ltd.	Ord	4/-	11/3
Contin (George), son a Co., Etc	410/ F D.E		14/6	Silement I wist Di ill di Steel Co., Etd.	014	1	ex right
Coventry Gauge & Tool Co., Ltd	Ord	10/-	14/3		5% Cum, Prf.	13	15/-
	5% Cum.	El	16/3	Stedall & Co., Ltd	Ord	5/-	6/3
	Red. Prf.			Tap & Die Corporation, Ltd	Ord	5/-	7/6
Coventry Machine Tool Works, Ltd.	Ord	5/-	8/3	es 11 11 11 1111111	41% Deb.	Sek.	82/-
Craven Bros. (Manchester), Ltd			6/71	Wadda Lad	1961-1977 Ord	10/-	17/6
Elliott (B.) & Co., Ltd		13	13/9	Wadkin, Ltd	Ord	10/-	79 /04
	Cum, Prf.	-		11 11 11 11 11 11 11 11 11 11 11 11 11	5% Cum.	EI	13/9
Export Tool & Case Hardening Co., Ltd.	Ord	2/-	1/3		Ist Prf. 5% Cum.	13	24/-
Firth Brown Tools, Ltd		EI	12/-		2nd Prf.	-	
Greenwood & Batley, Ltd	Ord	. [1	48/14	Willson Lathes, Ltd	Ord	1/-	2/41

The Middle Prices given in the list are in several cases nominal prices only and not actual dealing prices. Every effort is made to ensure accuracy, but no liability can be accepted for any error.

\* Sheffield price. † Birmingham price.

#### PRICES OF MATERIALS

P	RICES	,
Pig-Iron		
Foundry and Forge No. 3, Class 2		
Middlesbrough zone Birmingham	£21 6 £20 18	0
Phos. 0-1 to 0-75% Birmingham	£23 17	0
Scottish Foundry Grangemouth	€25 3	6
Hæmatite English No. I		
N.E. and N.W. Coast Scotland Sheffield	£25 6 £25 13 £26 15	600
Birmingham Welsh	£27 4 £25 6	6
Steel Products	-	
Madium places	y* £45 11	6 00
Mild steel plates, ordinar Boiler plates* †Flat bars 5 in. wide and u †Round bars under 3 in.	£44 12 inder } £40 6	6
Billets, rolling quanty, so	Æ U.T. £32 15	6
Phosphor Bronze Ingots (288) (A.I.D.)_d/d	£258 0	0
Copper	/207 T	
Cash (mean) Cold rolled and hot rolle 4 ft, by 2 ft, by 10 S	£207 7	6
	6271 15	0
Rods 1 in. to 1 in. diam Tubes, 11 in. bore by 10 ton lots, per lb. Wire rod, black, hot-rolle English	2s. 9 d (4-14 in.) £222 17	d. 6
Zinc		
Refined, minimum 98 per current month (mean)	cent. purity, £64 15	0
Brass		
Tubes, selid drawn, per li Strip 63/37, 6 in. by 10 SW ton lots £228 Rods, ‡-3 in. diam. (59 per	b. Is. 7½ 'G coils, 0 0—£230 10	
Rods, 4-3 in. diam. (59 pe copper)	1s. 9%	d.
Yellow Metal		
Condenser plates, per too Rods, per lb.	1 6165 0 ls. 10%	0 d.
Aluminium		
Ingots min. 99-5 per cent Canadian d/d	£180 0	0
Lead		
Refined, minimum 99-97 purity, current month (		6
Tinplates		
†U.K. Home trade: Handmill f.o.t. makers' Cold reduced, f.o.t. ma works	Kers'	_
IIK Exports		-
Hot rolled basis, f.o.t. works' port Cold reduced basis, f.o. works' port	72s. 6d.—75s. 0d t. 75s. 0d	
Gunmetal		
Ingots, 85.5.5.5. ex works * N.E. Coast, N. Join Scottish Zone. † U.T. soft basic.	£168 0 t Area, Centra	
† U.T. soft basic.	after allowing fo	

‡ Official maximum price, after allowing for adjustments for increase in price of tin.

F MA	<b>TERLA</b>	LS
MAK	ERS' PRICE	S
Hexagon St	nel Bars <sup>1</sup>	
	from I in. up	
	1-41 a/f, ex work	
2 ton basis	a ale	£42 17 0 £47 6 6
Free cutting blo	BCK	24/ 0 0
Reeled Steel	Bars1	
f.o.t. works	+ in. upwards	1
for sizes) Free cutting		£43 9 6 £47 19 0
High-Speed	Steel	
	length bar. Al per lb., subject	
Molybdenum "	66 "	5s. 104d.
Molybdenum "	46 "	5s 8id.
14 per cent tur	igsten	5s. 9d.
16 per cent tur	gsten	6s. i d.
18 per cent tur	gsten	6s. 4d.
22 per cent tur	igsten	7s. 5d.
+ 6.0/6.75 per	it ent molybdenum cent tungsten + cent vanadium	
Precision-gro		
	ning Brass F	
1-in. dia. ± 0	·00025-in. 2-tor	2- 471
lots, per lb.		2s. 42d.
Grey Iron R	od	
18 in. to 26 in 18 -in. above if for definite	random lengths rough machined listed size. Extra lengths. Dis- rders over £150	
	Perc	wt. net.
A no Y in	Mark I	Mark III
for fin.	245s. 4d. 196s. 4d.	318s. 10d. 251s. 10d.
I to I in.	137s. 10d.	171s. 2d.
It to 2 in.	106s. 2d.	125s, 11d,
24 to 34 in.	91s. 6d.	106s. 4d.
31 to 31 in.	91s. od. 86s. 6d.	99s. 2d.
28 EO 17 IU	805. 6G.	775. ZG.

	Per c	wt. net.	
	Mark I	Mari	k III
d or d in.	245s. 4d.	318s.	IOd.
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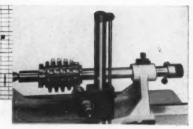
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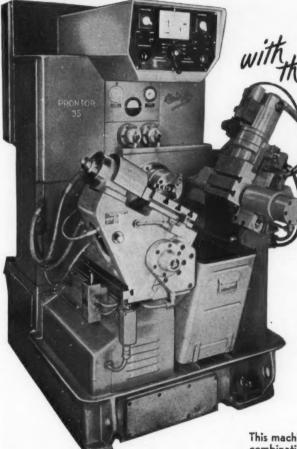
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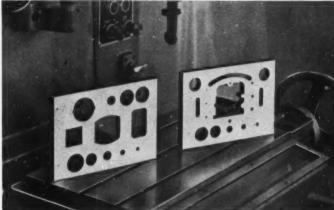
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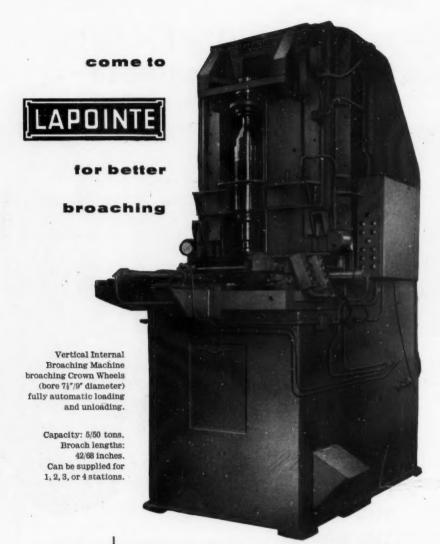


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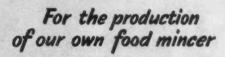


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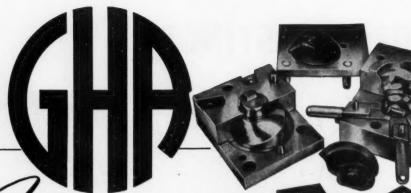
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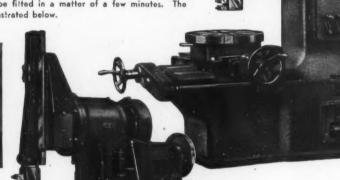
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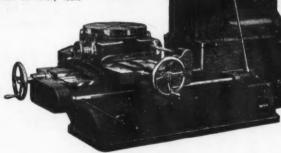


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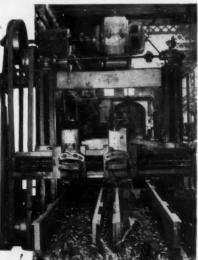
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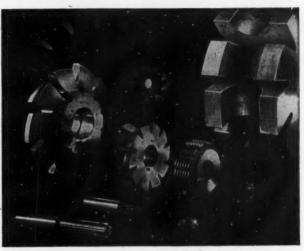
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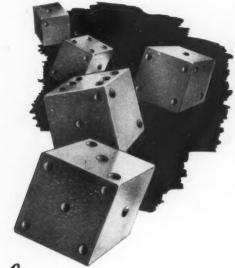
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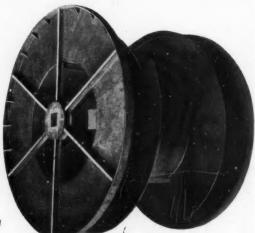
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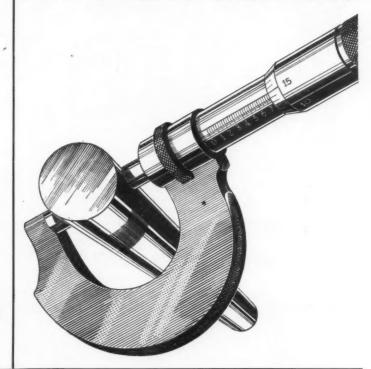
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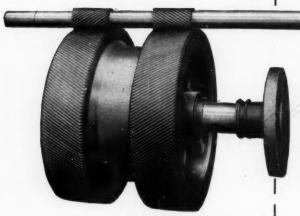


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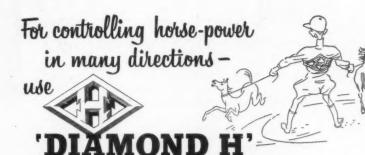
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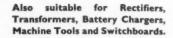
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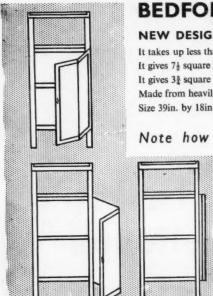
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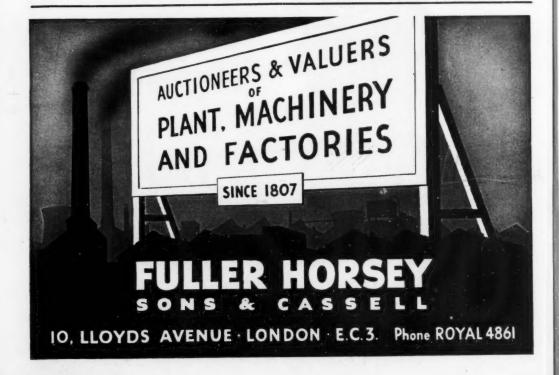
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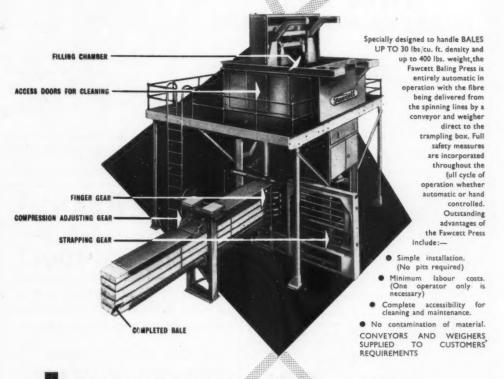
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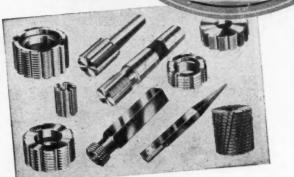
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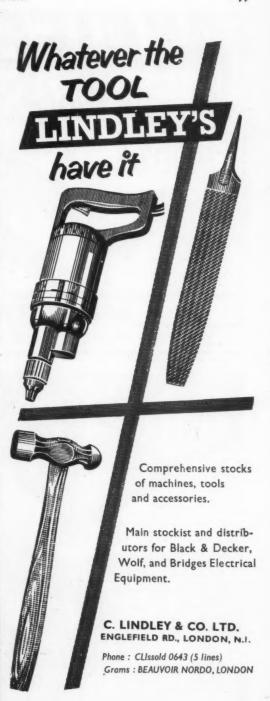
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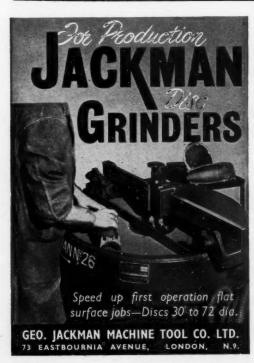
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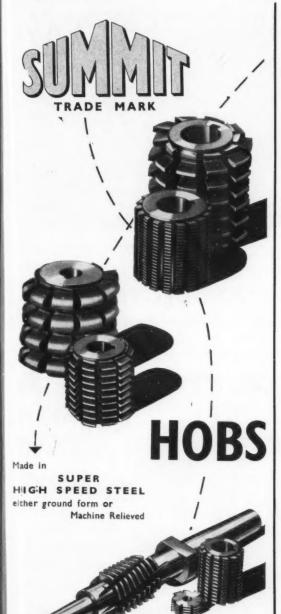
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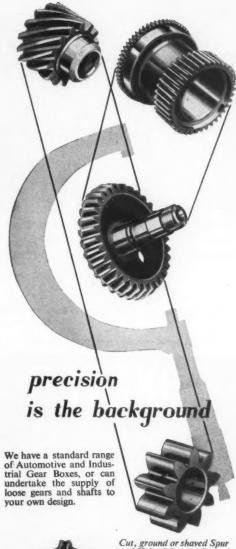


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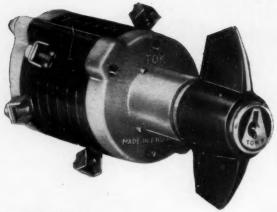
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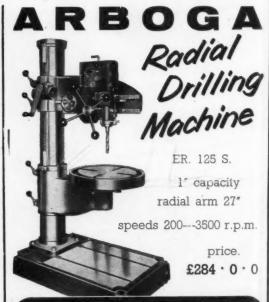
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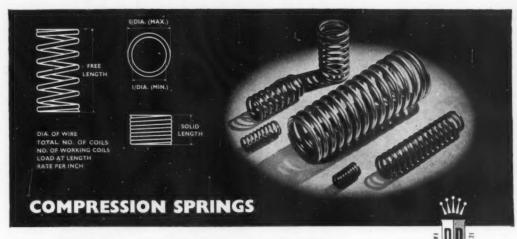


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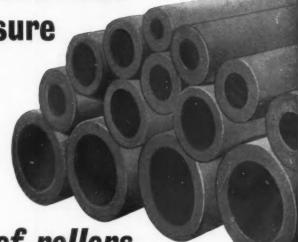
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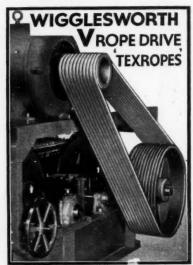
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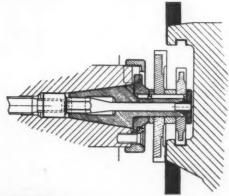
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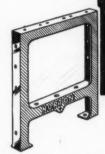
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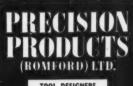
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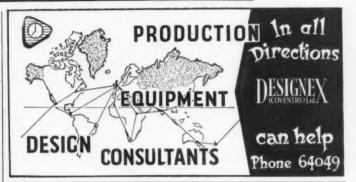
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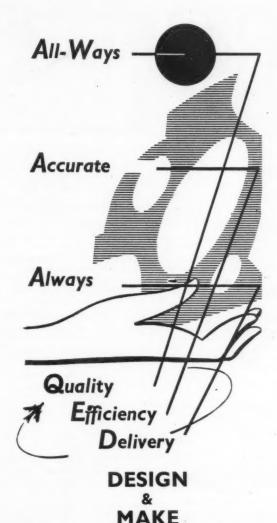
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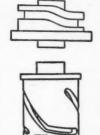
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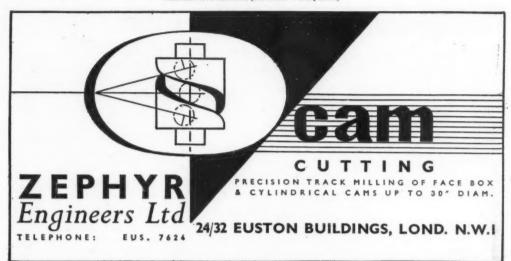
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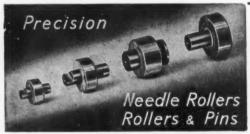
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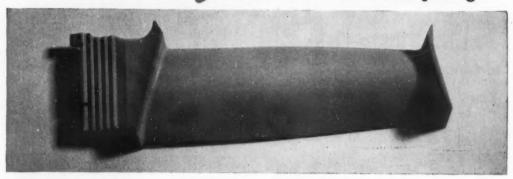
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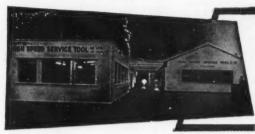
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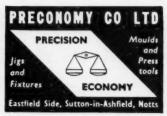
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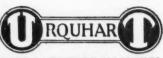
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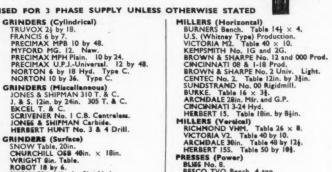


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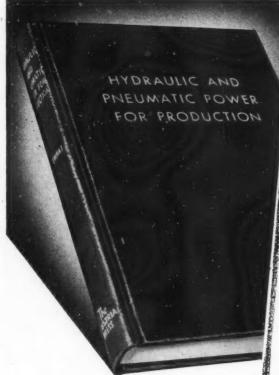
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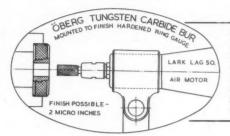
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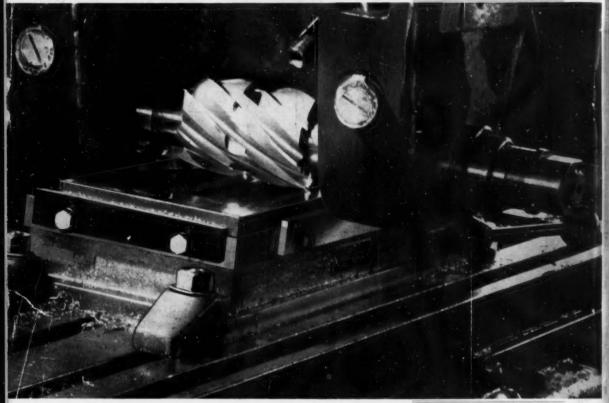
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# magnetic chucking



# for greater gripping power

gripping right across face, side grip as well

total magnetic power unsurpassed

The operation shown illustrates an excellent example of the use of Magnetic Chucks on milling machines. A mild steel plate measuring  $11^{\circ} \times 5^{\circ} \times \frac{1}{2^{\circ}}$  is accurately located by means of the Magnetic Chuck side and end stop plates. Two recess reliefs each measuring  $1\frac{1}{2^{\circ}}$  wide by  $\frac{1}{2^{\circ}}$  deep are then gang milled using a cutting feed of  $3\frac{1}{2^{\circ}}$  per min. The cutting stroke is 8° long, complete floor to floor time of  $4\frac{1}{2^{\circ}}$  min. Setting and clamping time is completely eliminated.



light-durable-strong

end & side stop for easy, rapid setting

precision ground surface



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